



Variable Angle Target Training System

(V.A.T.T.S.)

TEAM #16

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DESIGN REVIEW #2

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Overview



- Background
- NewArm Analysis
- System Mock-up
- Budget & Purchase
- Future Work

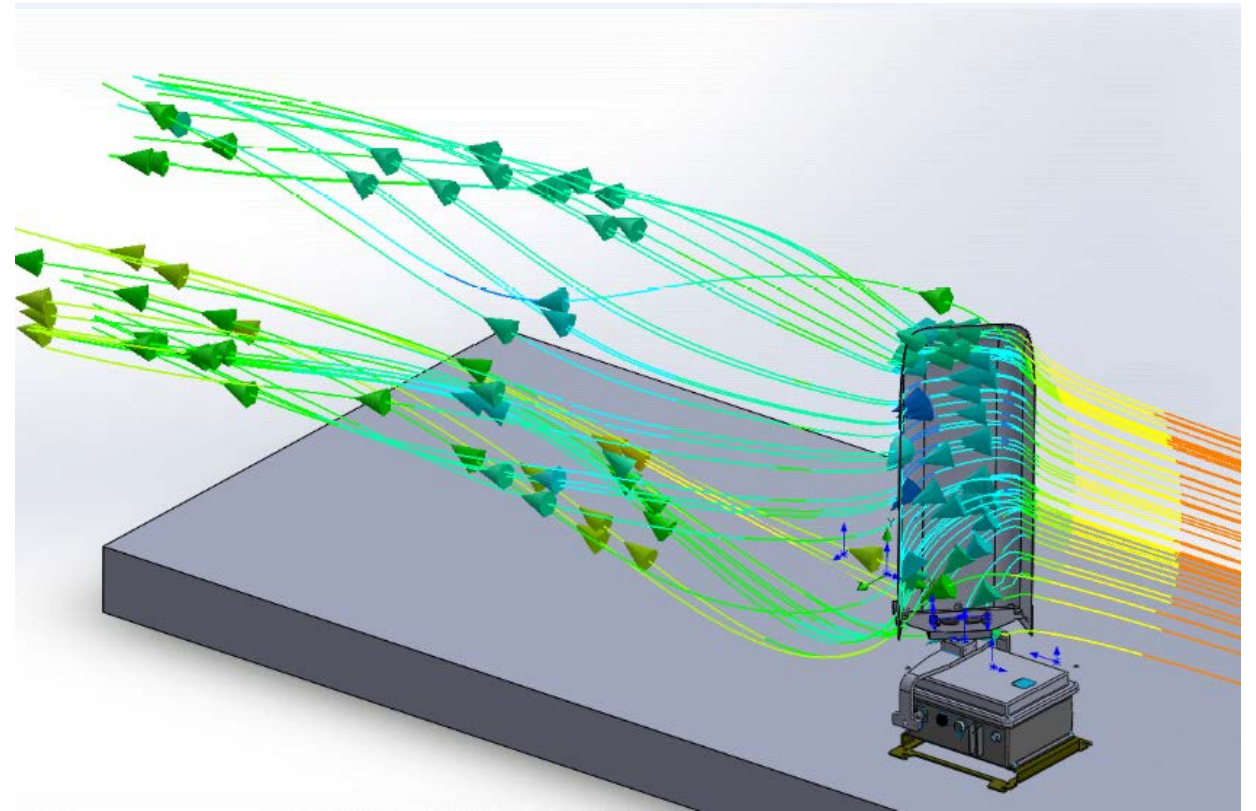


Fig. 1

Background

- Stationary Infantry Targets (SITs) are used to train military in combat situations
- Include many features that help provide a more realistic experience
 - Muzzle Flash
 - Hit Detection
- Flips targets up and down
- A variety of targets can be used with the SIT



Fig. 2

Background



“E” Style
(Waffle Board)
Fig. 3



“Figure 12”
Style
Fig. 4



“Figure 11”
Style
Fig. 5

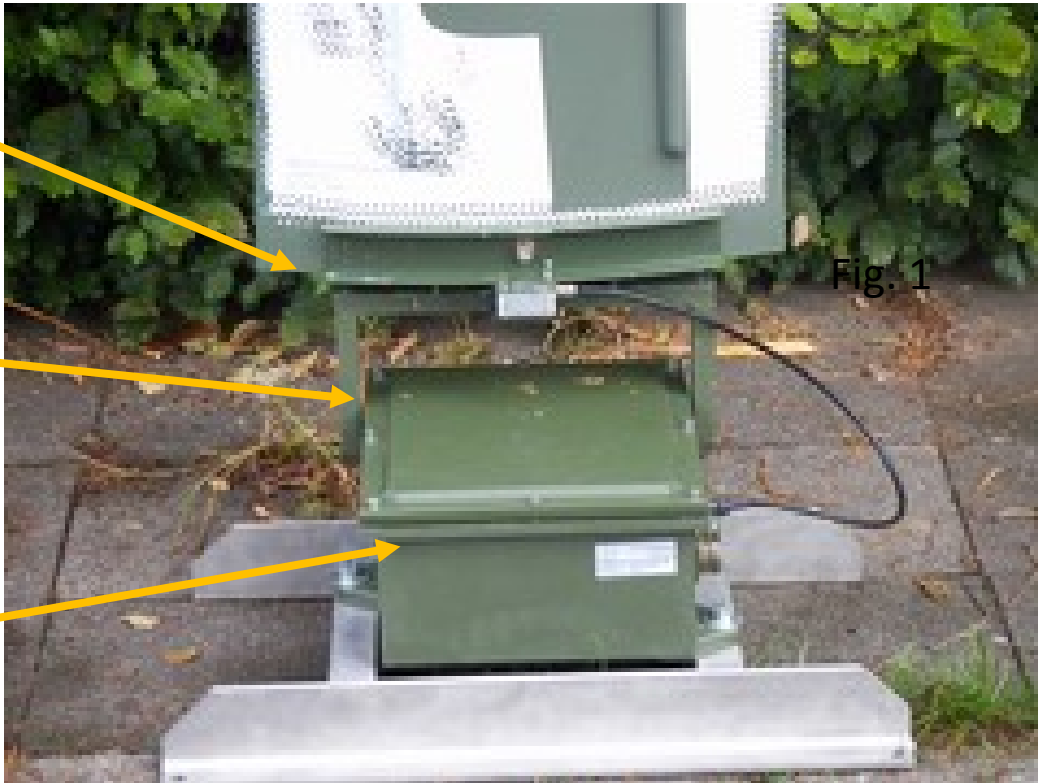


“Ivan”
Style
Fig. 6

Terminology

Target
Bracket

Arm



Lifter

Fig. 1

Fig. 7

Friend & Foe

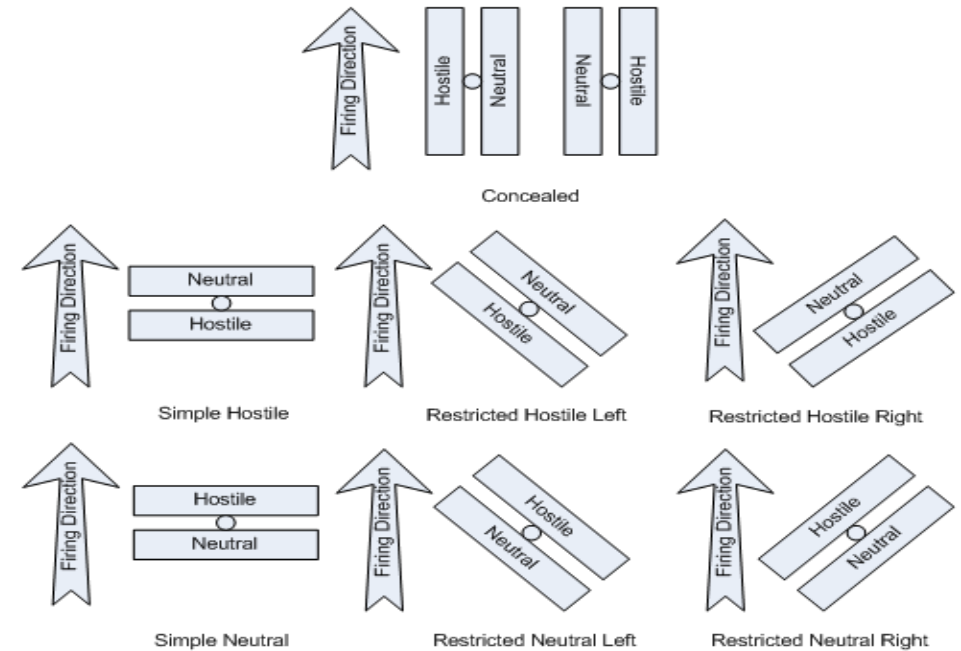


Fig. 8

Needs and Goal Statement

- Needs Statement:

“Lockheed-Martin’s current Stationary Infantry Target does not allow for horizontal rotation.”

- Goal Statement:

“To create a target system that can deploy a variety of targets from a resting position, and rotate to a desired angular position.”



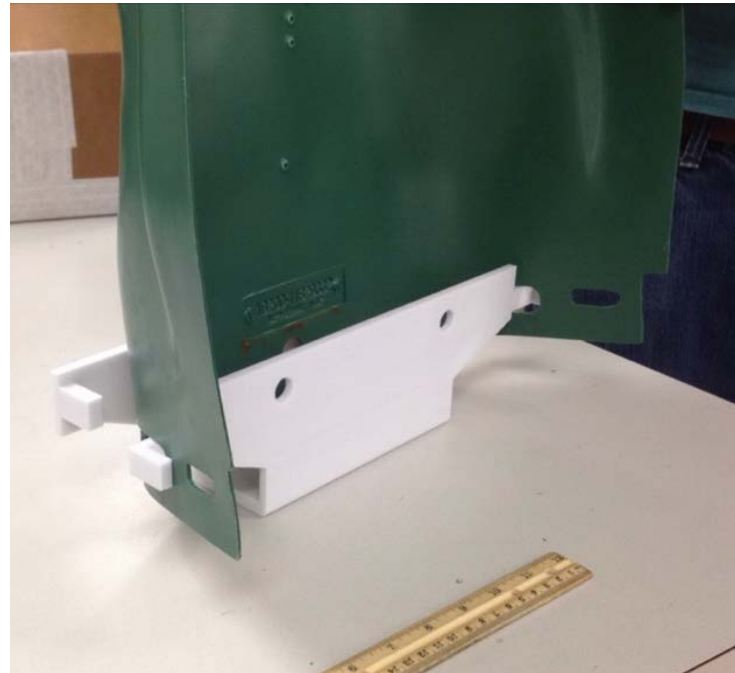
Design Progress

- The 3D printed bracket has been received from Lockheed
- Arm and Bracket Design changed based on our 3D printed prototype



“E” Style (Waffle Board)

Fig. 11



“Ivan” Fit

Fig. 12



“Figure 12” Fit

Fig. 13

Bracket Design

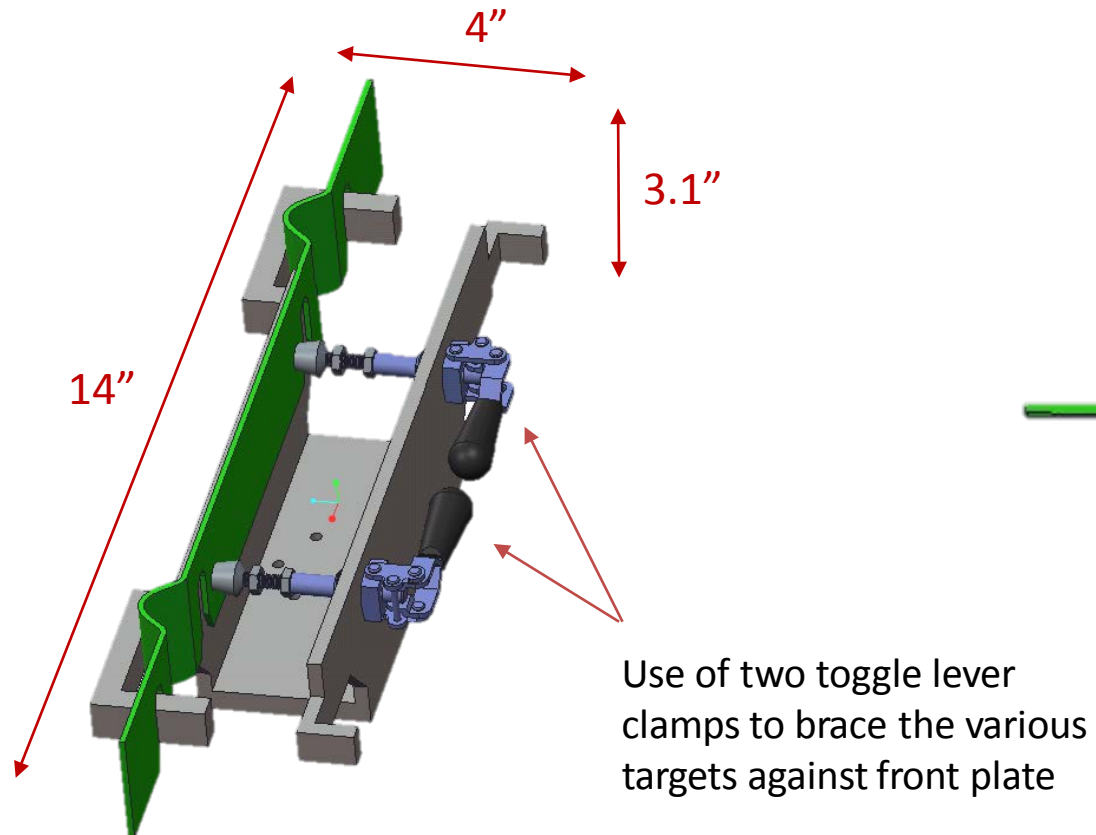


Fig. 14

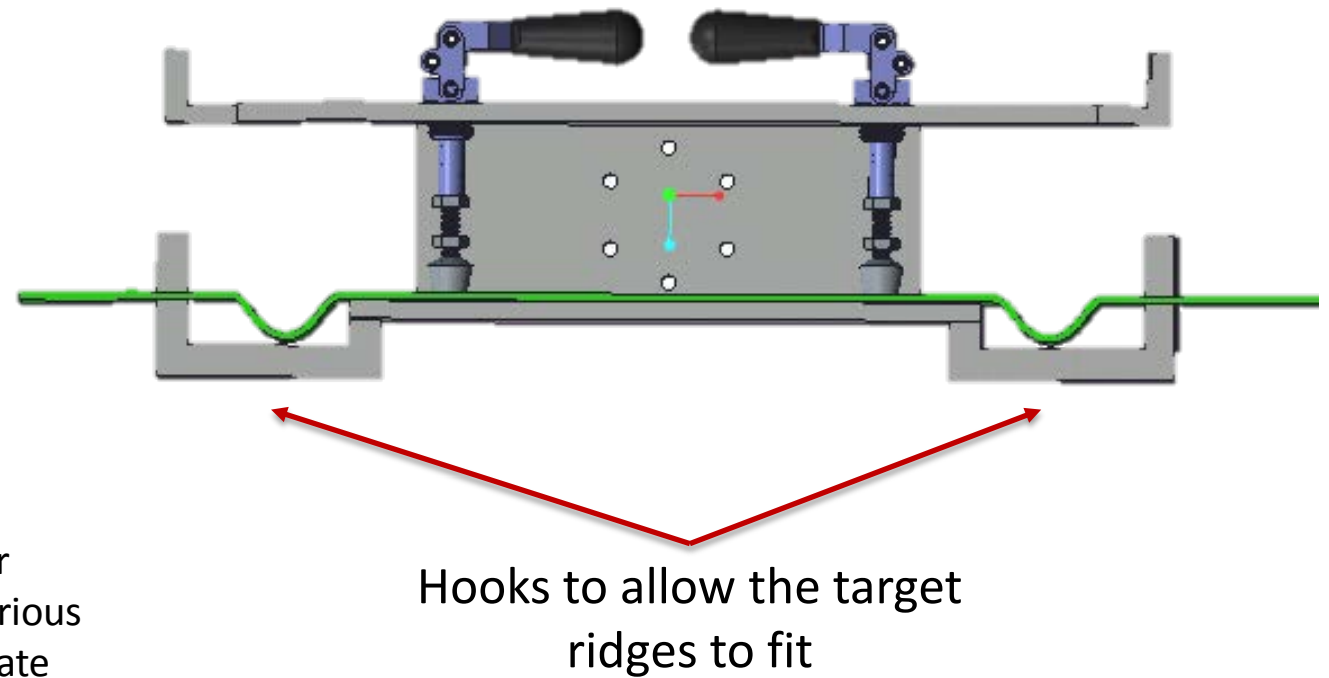
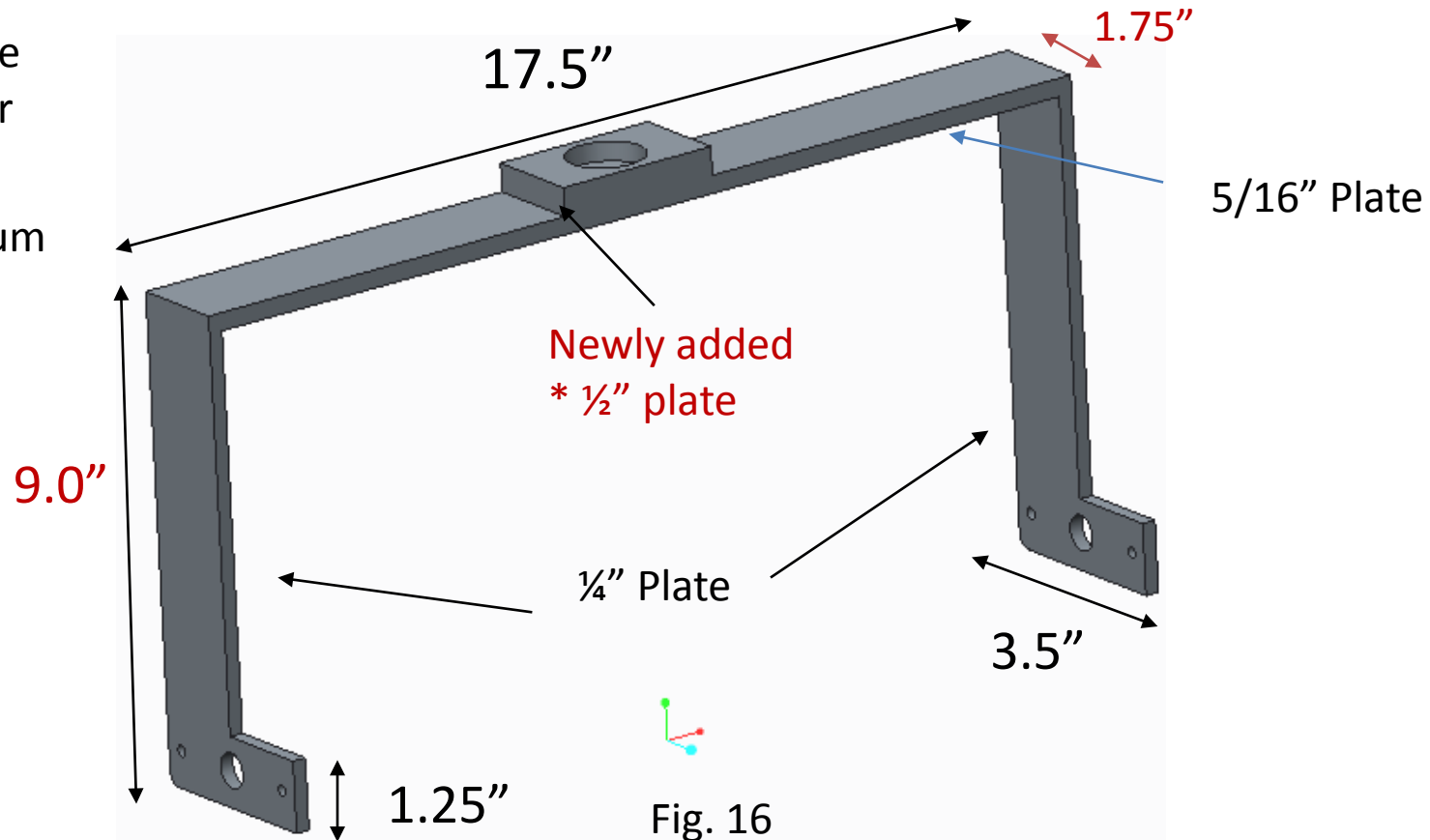


Fig. 15

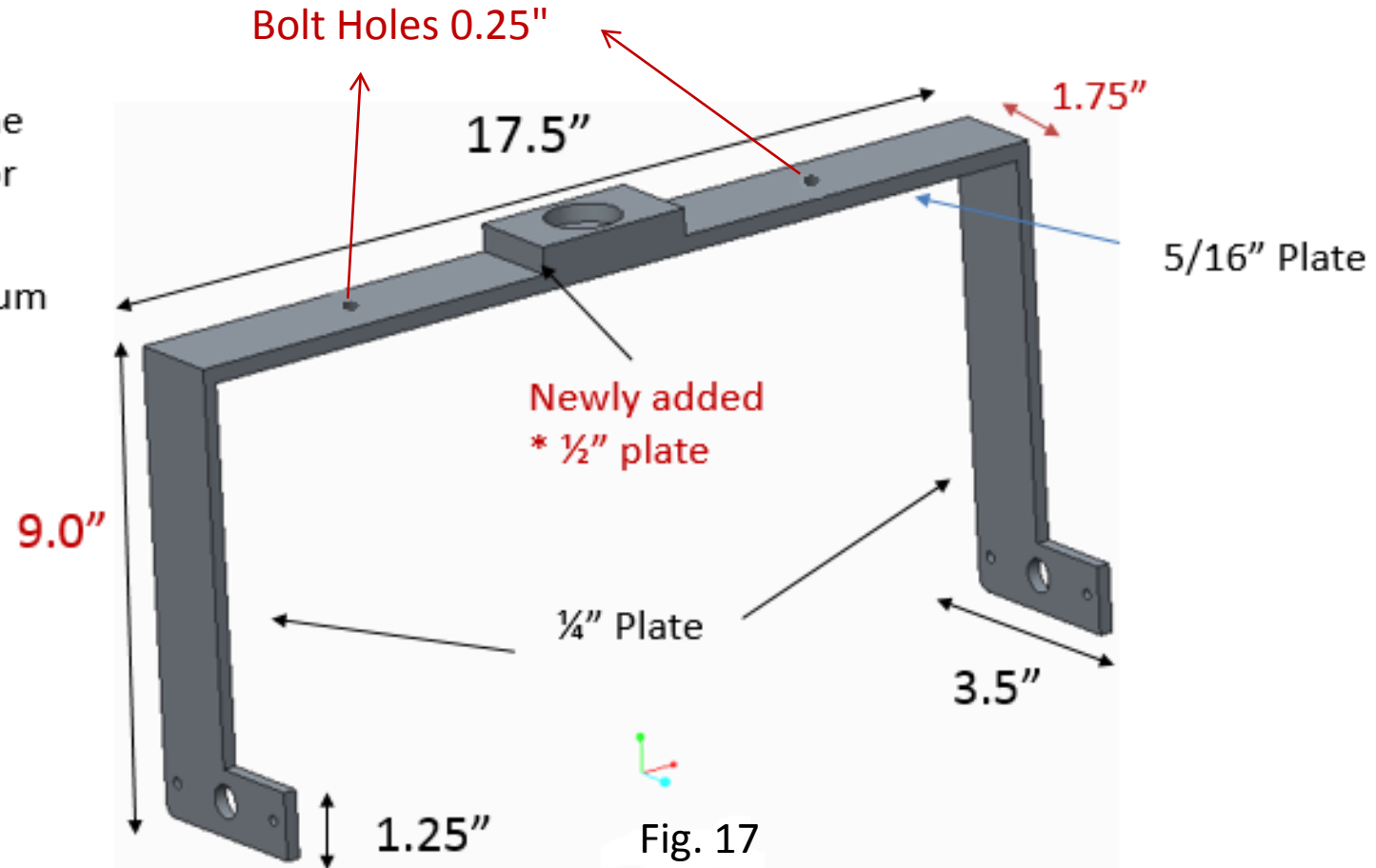
Previous Arm Design

- * Welded to top of the arm to allow space for bearings
- * All Material Aluminum 6061



Current Arm Design

- * Welded to top of the arm to allow space for bearings
- * All Material Aluminum 6061



Bracket Analysis



Fig. 18

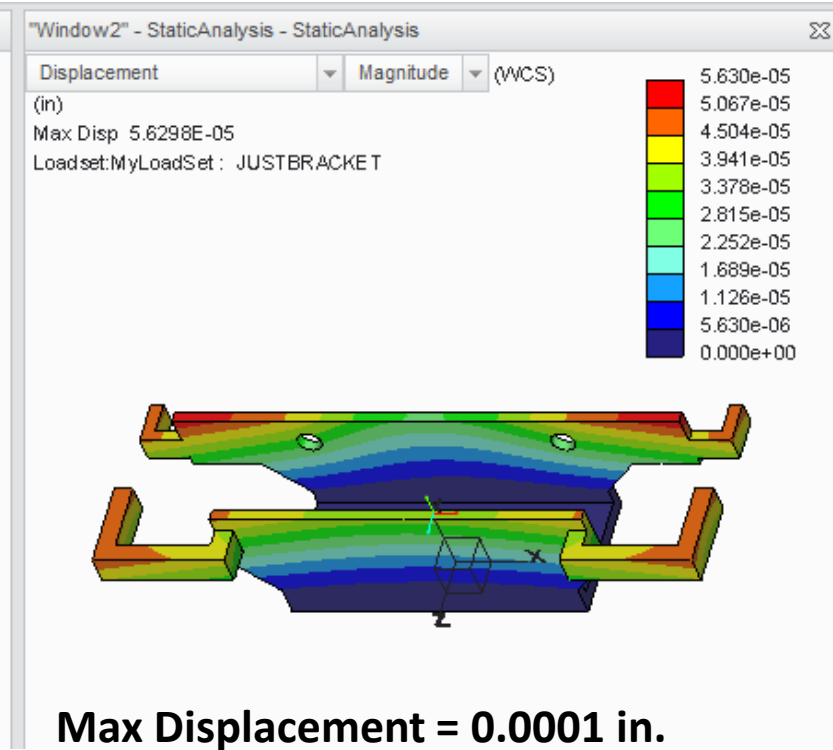


Fig. 19

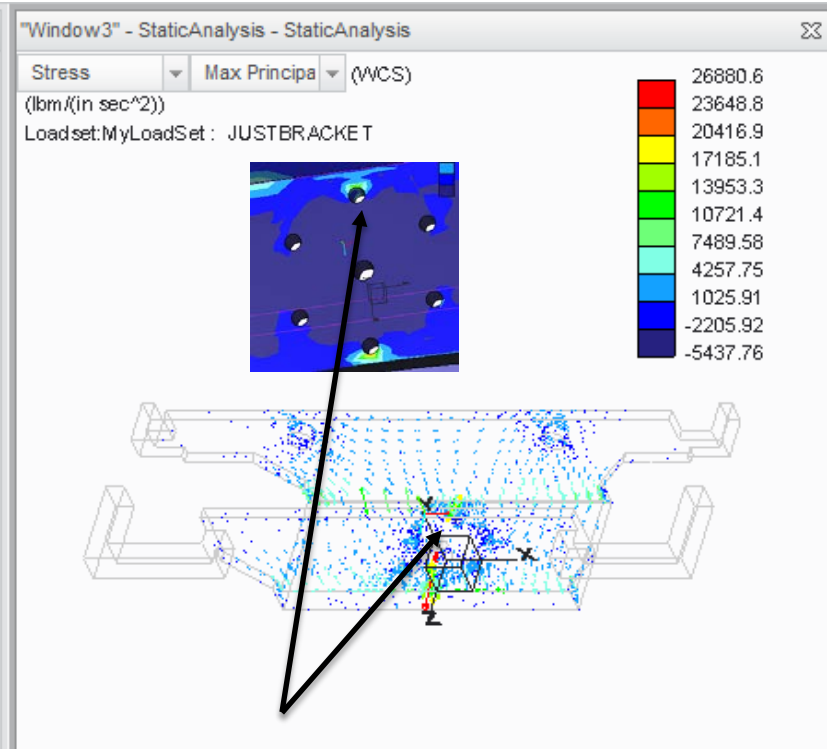
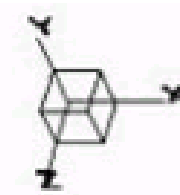


Fig. 20



Arm Analysis

Worst case scenario
causing torsional
effects on arm

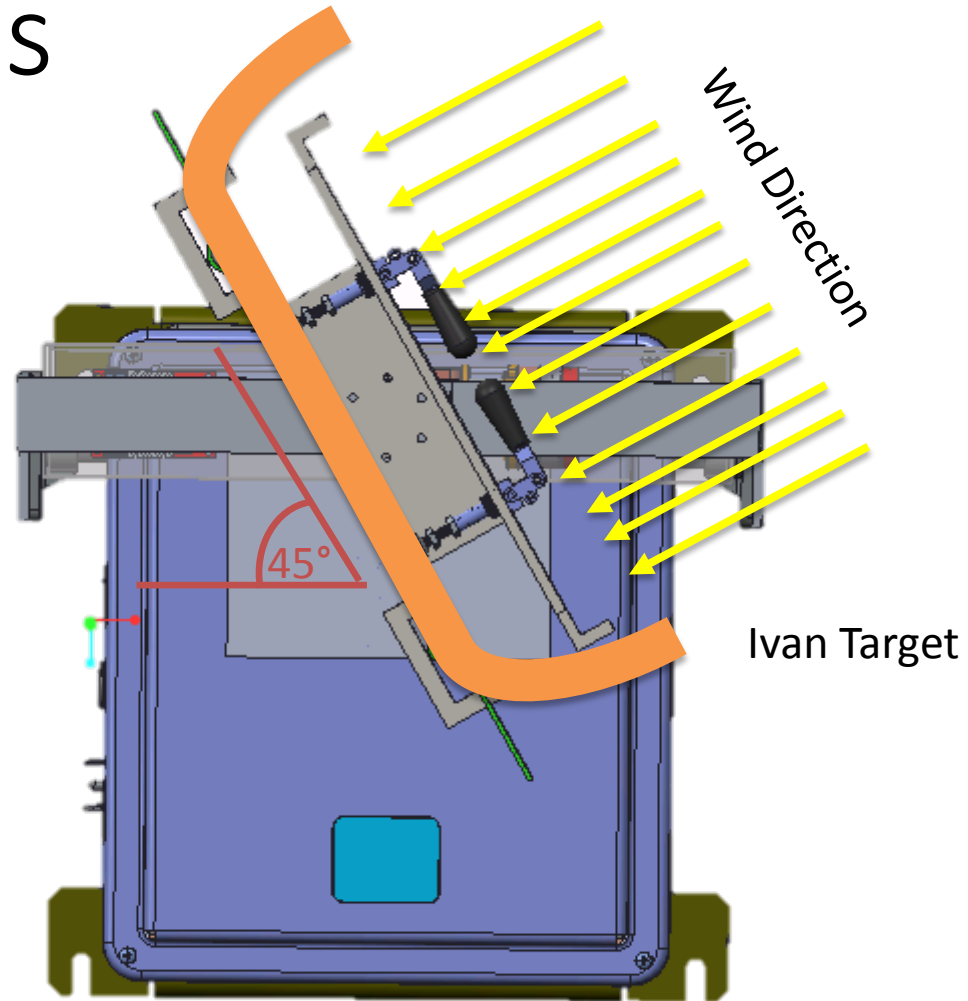
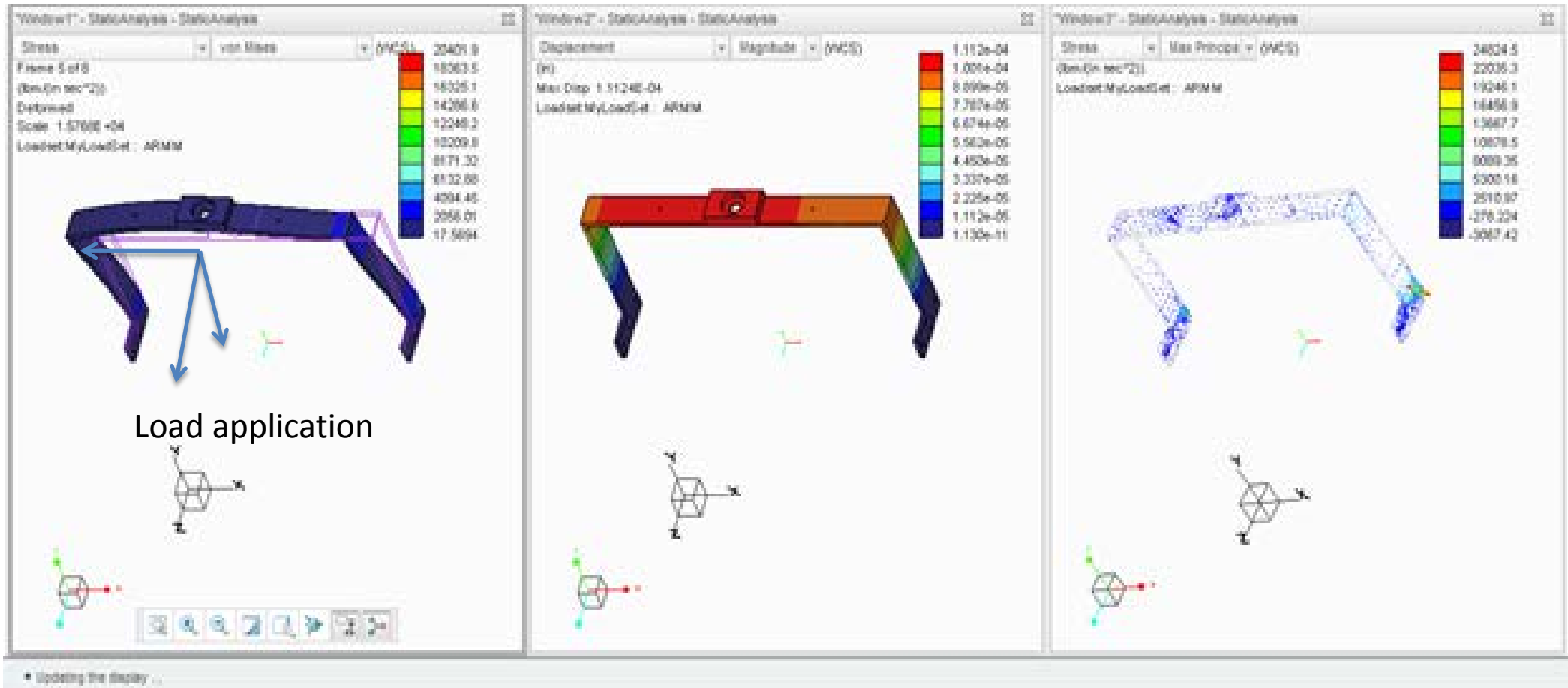


Fig. 21



Load application

Max Stress = 21,566 psi
Yield Strength = 40,000 psi

Fig. 22

Max Displacement = $1.8 \cdot 10^{-4}$ in
<(0.0001in)

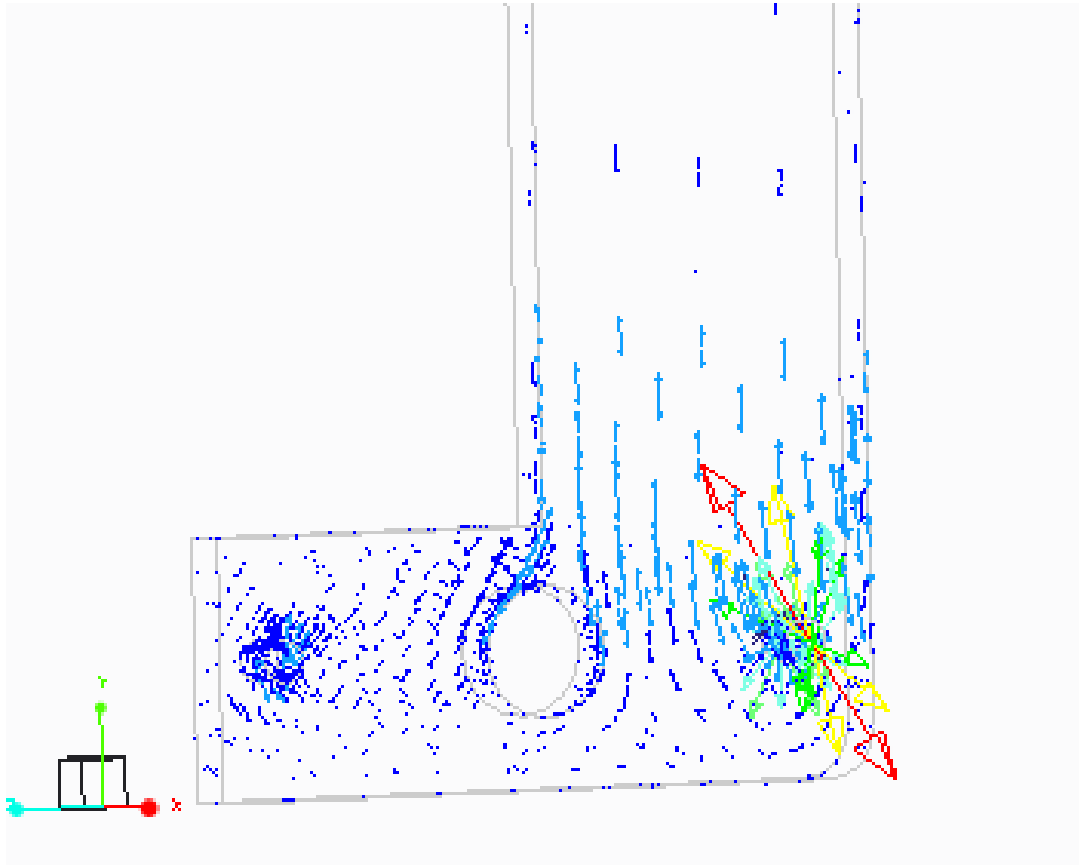
Fig. 23

Max Principal Stress Locations
on “Dog leg”

Fig. 24

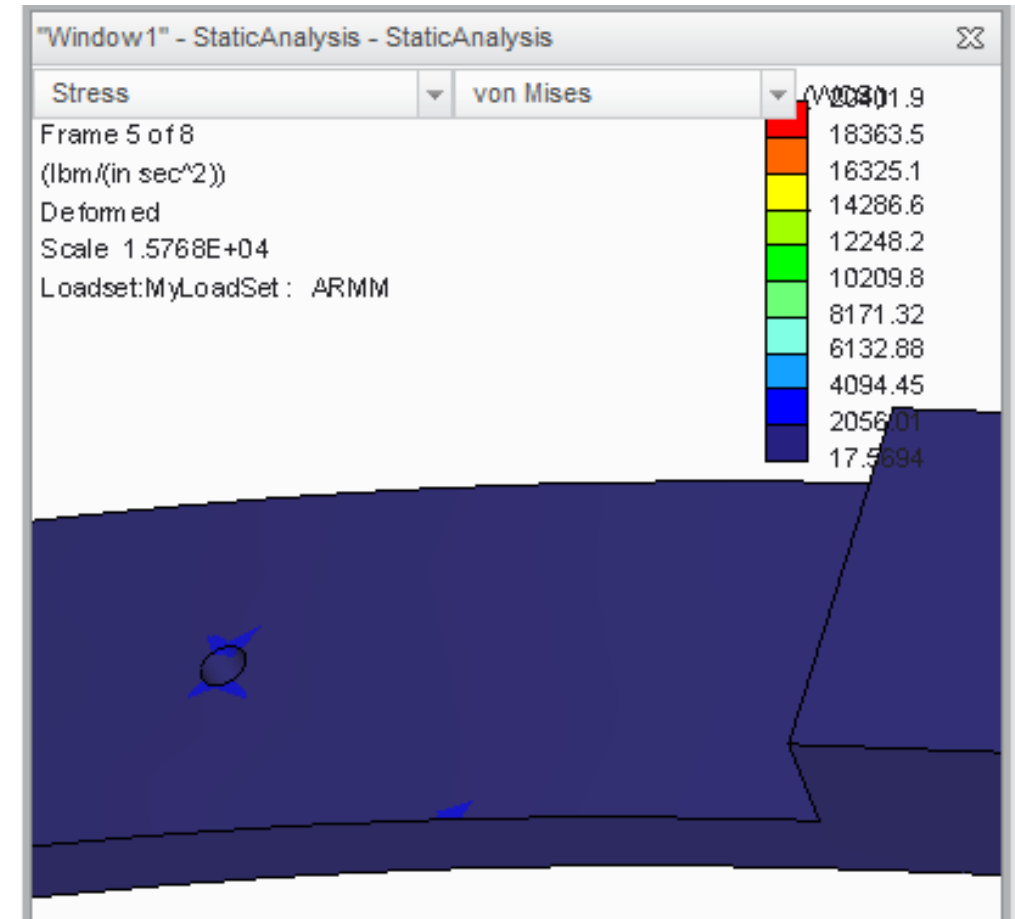


Arm Analysis



Arm Leg Stress Point
21,566 psi

Fig. 25



Bolt Hole Stress Point
Max Stress: 4,300 psi

Fig. 26

Turning Mechanism Specs

- Main values of interest to find Torque is inertia of the bracket and attached target as well as any forces generated by gust winds
- With a safety factor of 1.25 we found that we needed **3000 ozf-in @ 40 rpm**

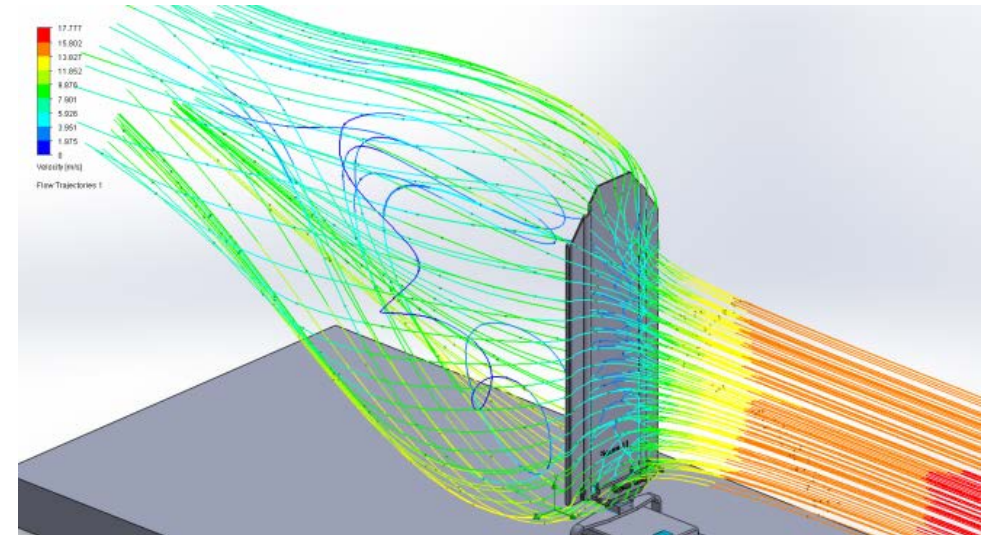


Fig. 27

Turning Mechanism Selection

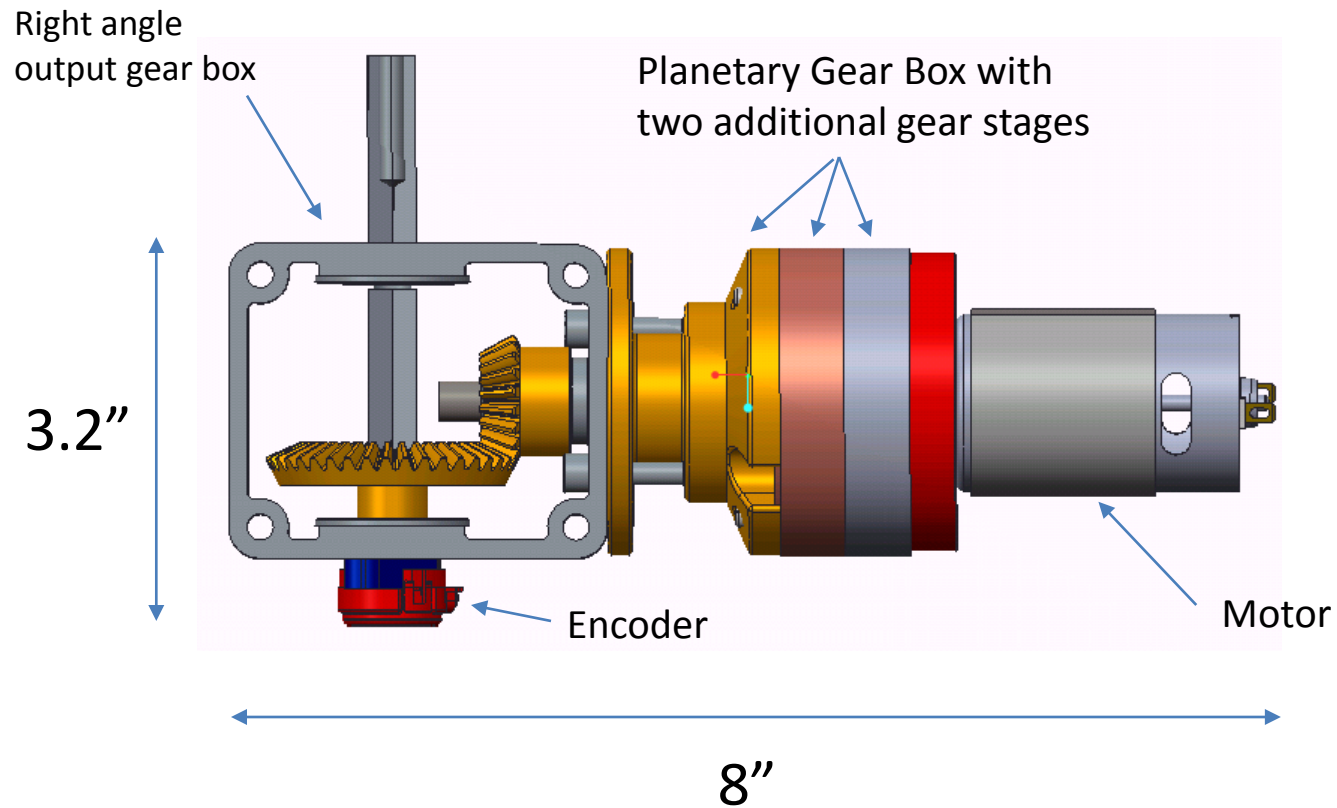


Fig.28

- Total Weight: 2.6 pounds
- Output of the right angle gear box:
 - Torque: 3000 oz-in
 - 80 RPM

Motor Enclosure

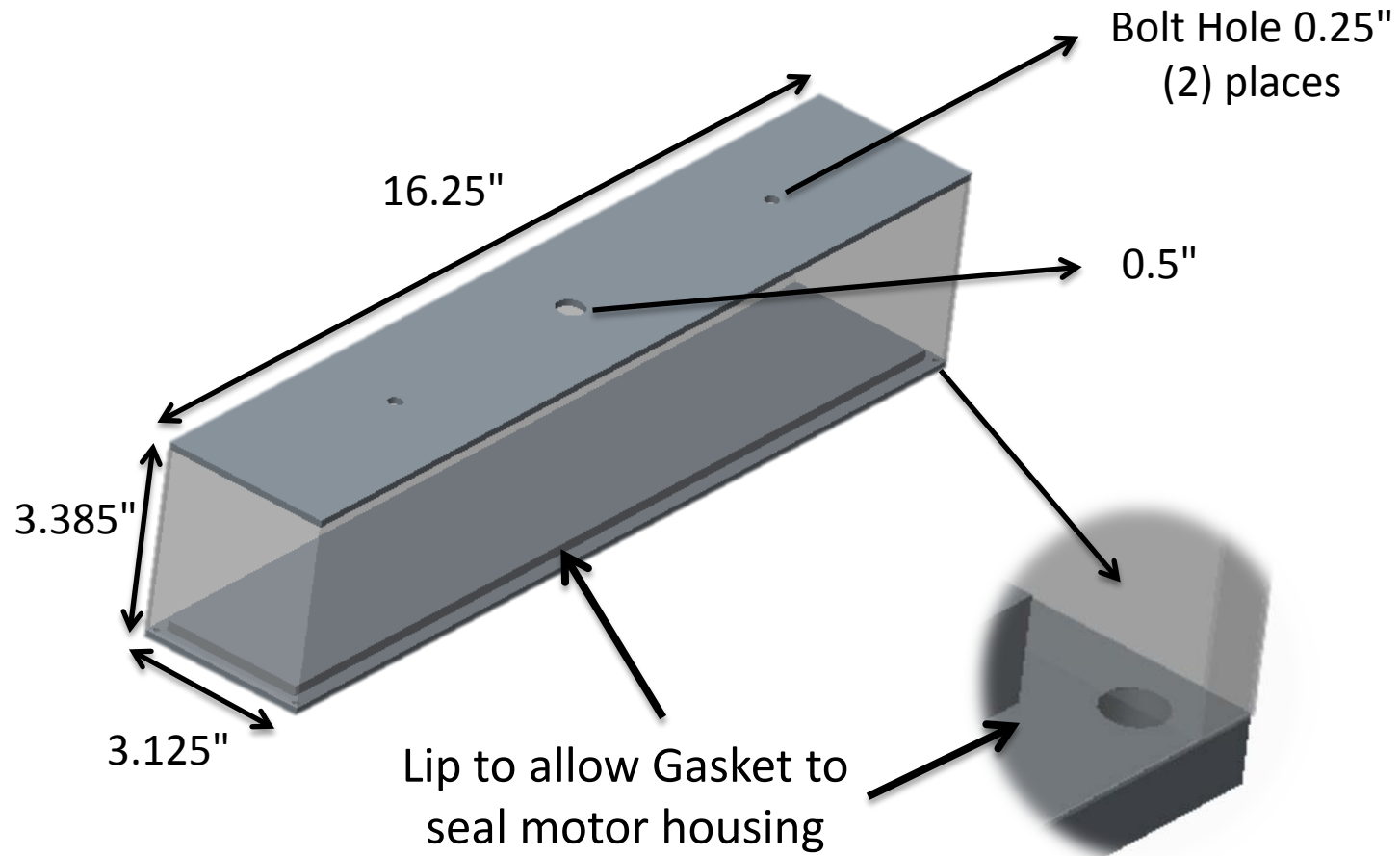


Fig. 29



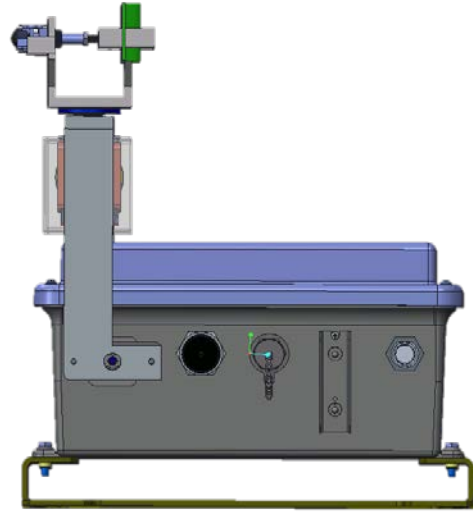
High Temperature Silicone
Adhesive Gasket Seal

Fig. 30

Finalized Design

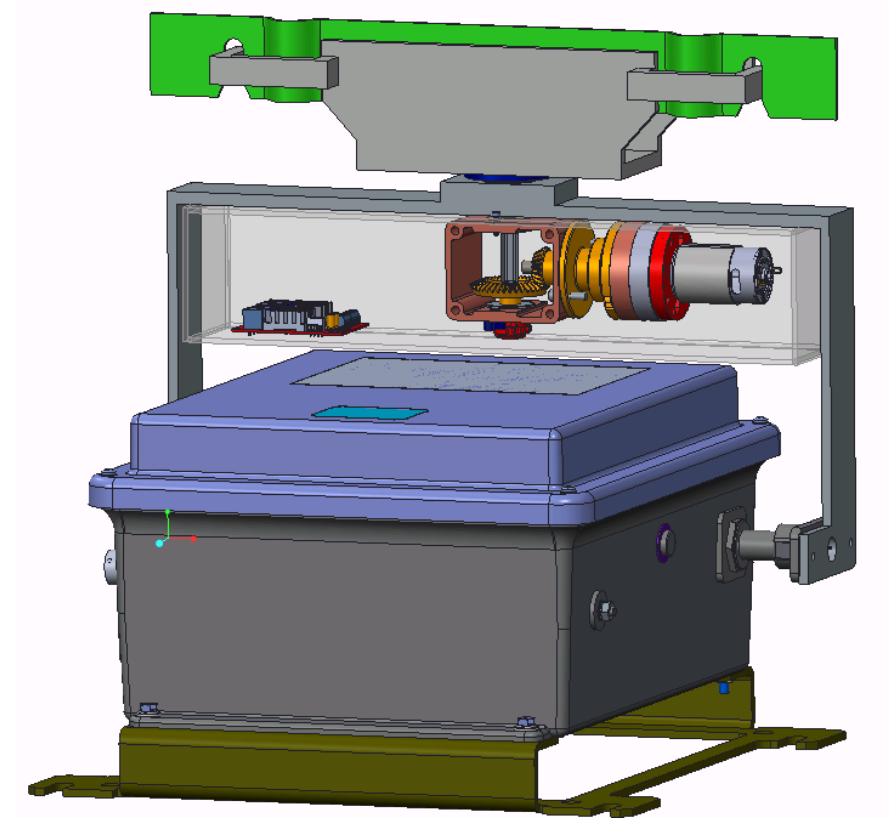
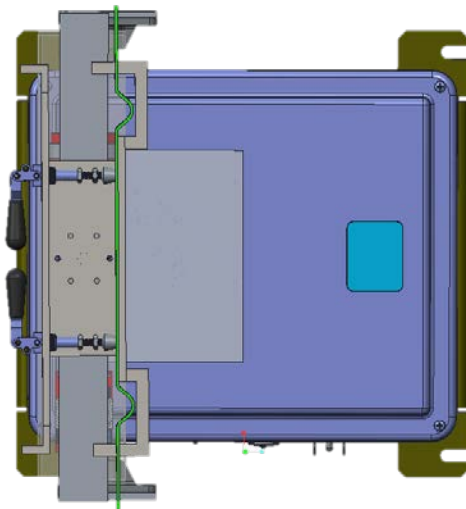
Side View

Fig. 31a



Top View

Fig. 31b



Parametric View

Fig. 31c

Finalized Design

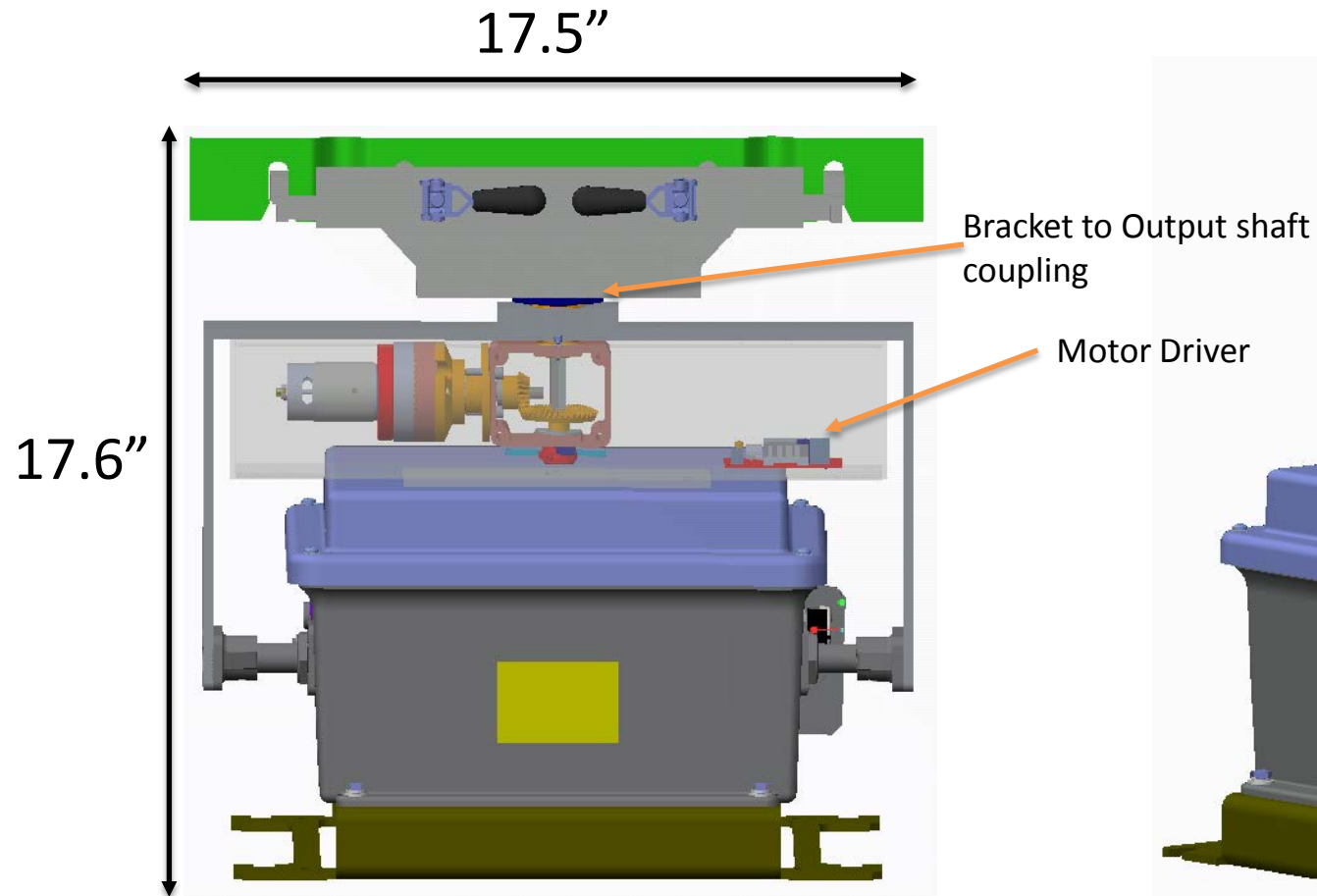


Fig. 31d

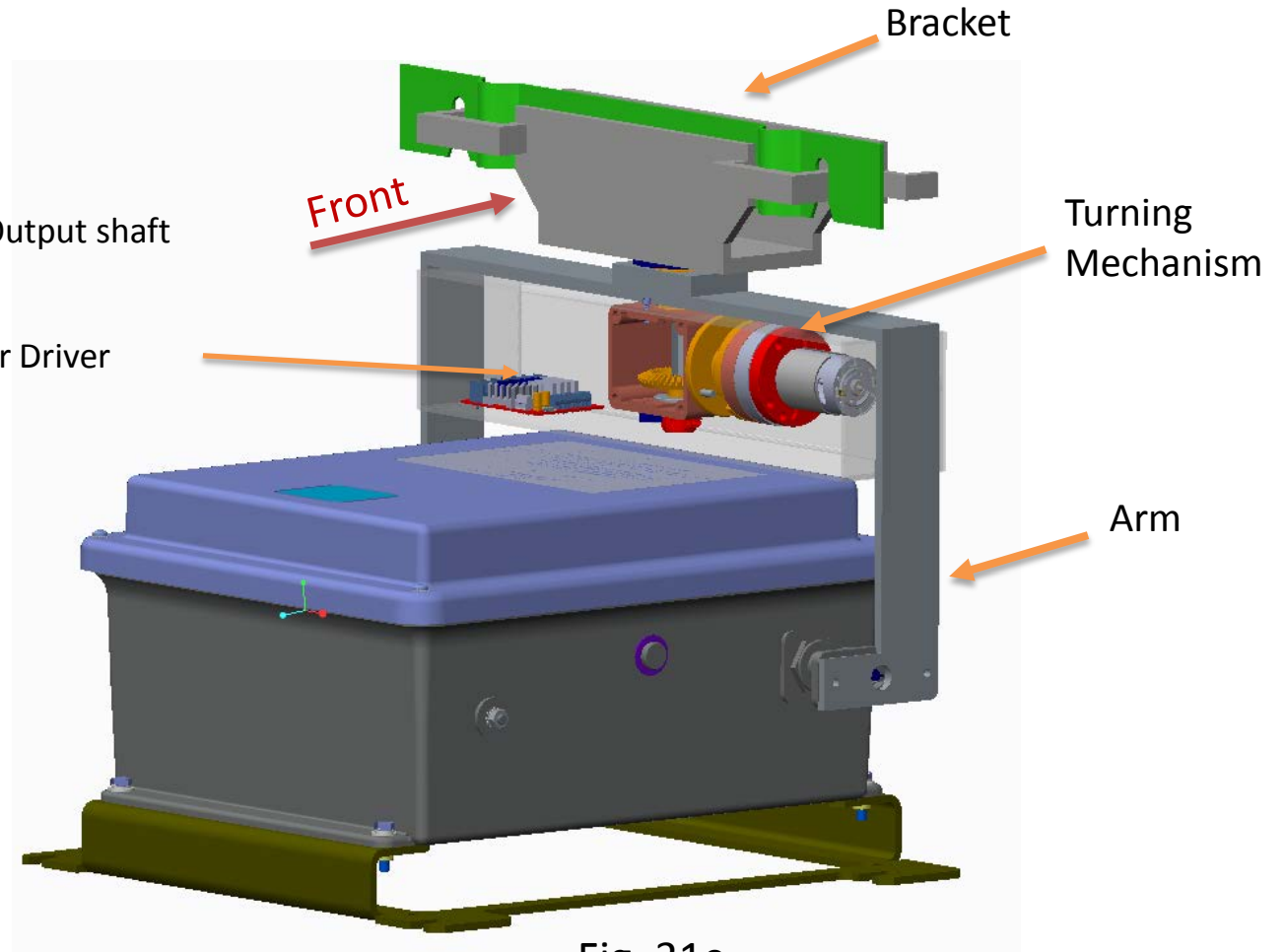


Fig. 31e

Aluminum Die Casting

Key Design Elements

- **Draft:** Anytime one have two halves of a die cast mold closing. For die casting a draft of at least 1 degree on any vertical wall.
- **Radii/Fillets:** Sharp edges on the die casting are generally not preferred. Typically a 0.030" minimum radius or fillet is preferred

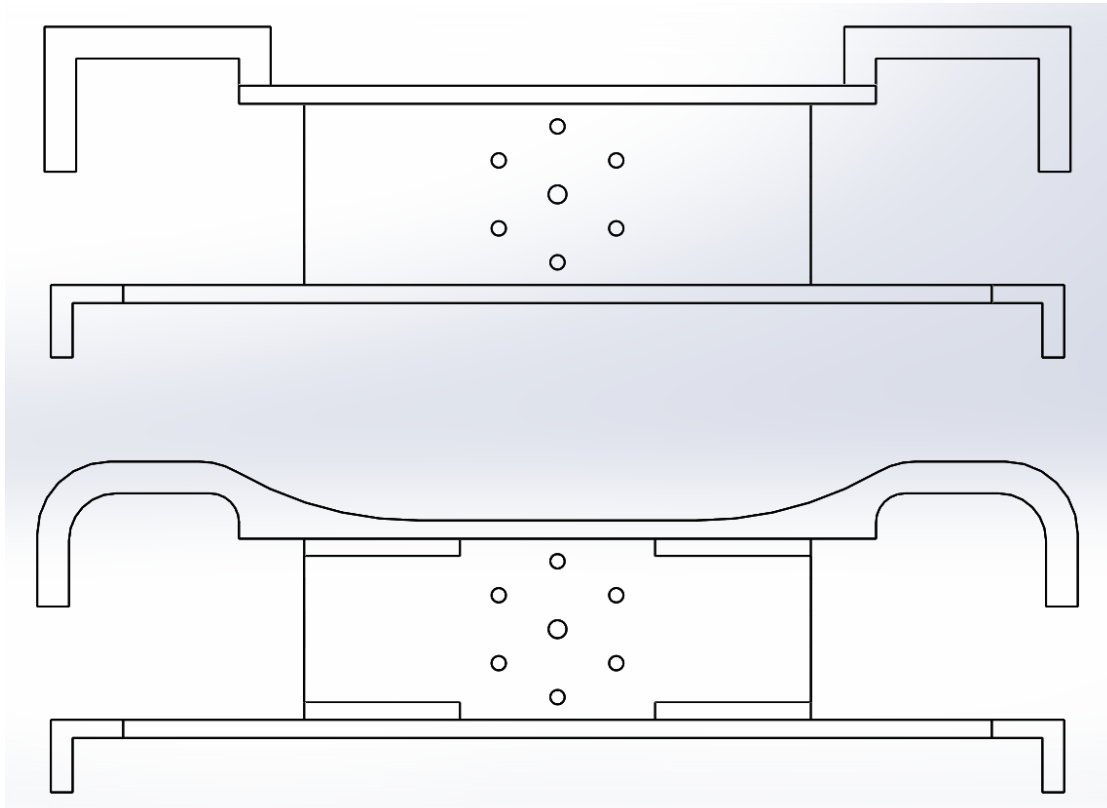


Fig. 32

Turning Control

- Team 11 has lent us an Arduino Mega 2650
- Arduino PID library and open source code to be implemented
- Mock up currently being developed

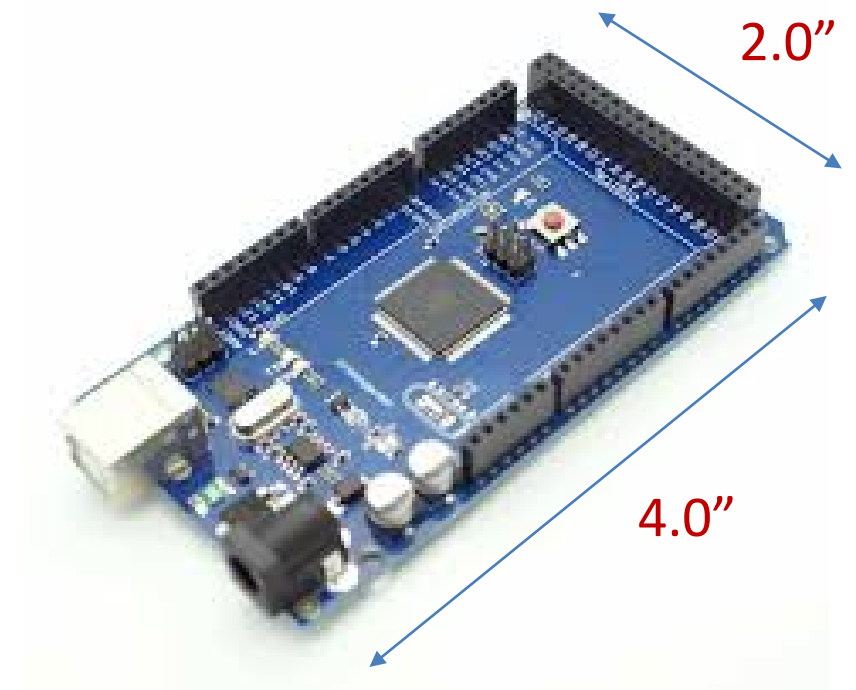


Fig. 33

Turning Control

- Require a high amperage motor driver (>32A continuous)
- Roboclaw 2x45A Motor Controller compatible with Arduino

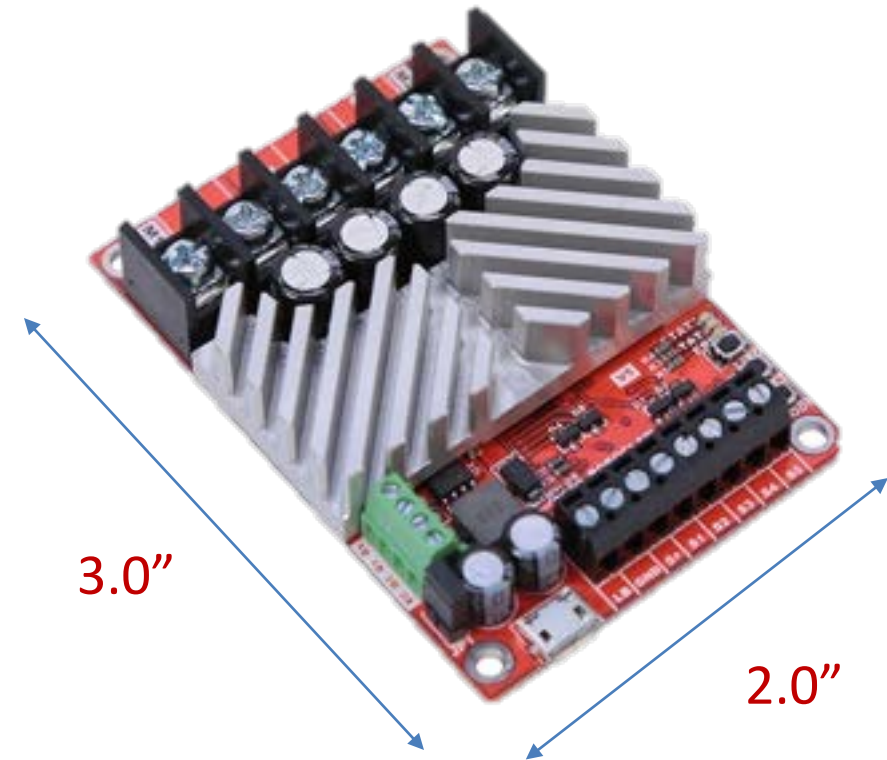


Fig. 34



Purchases

Date	Vendor Info	Item Description	Status	Total
Old Orders				
11/1/2015	n/a	Team travel to Lockheed Martin	n/a	167.81
12/2/2015	OnlineMetals	Aluminum plates and sheet	Delivered	164.99
2/9/2016	McMaster	Clamp with holder and bearing	Delivered	75.36
2/10/2016	AndyMark, Inc	Gearbox, motor and others	Delivered	439.22
New Orders				
2/24/2016	AndyMark, Inc	Screws and hex hub	Delivered	38.22
2/24/2016	OnlineMetals	Aluminum plates	Delivered	53.31
Upcoming Orders				
		Driver with controller	Not placed	
		Plexiglass and enclosure gasket	Not placed	
		Microcontroller	Not placed	

Budget: \$2000

Total exps: \$938.91

Remaining: \$1061.09



Summary

- Analysis performed on new arm
- Created Motor Enclosure with high temperature silicone gasket
- Structural and target turning components selected and ordered

Future Work

- Ordering Components:
 - Motor Driver
 - Motor Controller
- System Mock-up
- Machining raw material



Fig. 35

Questions / Comments

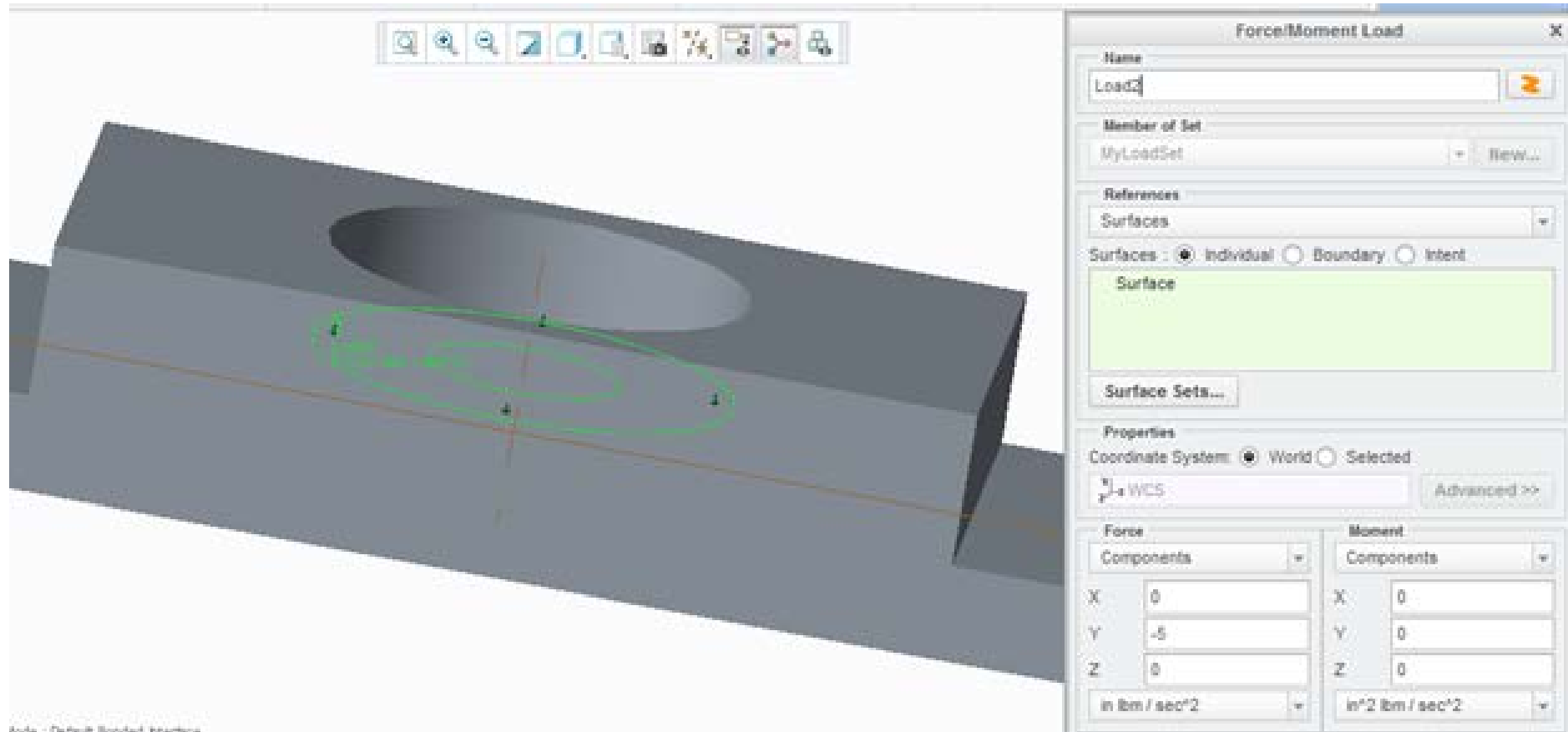


Fig. 36

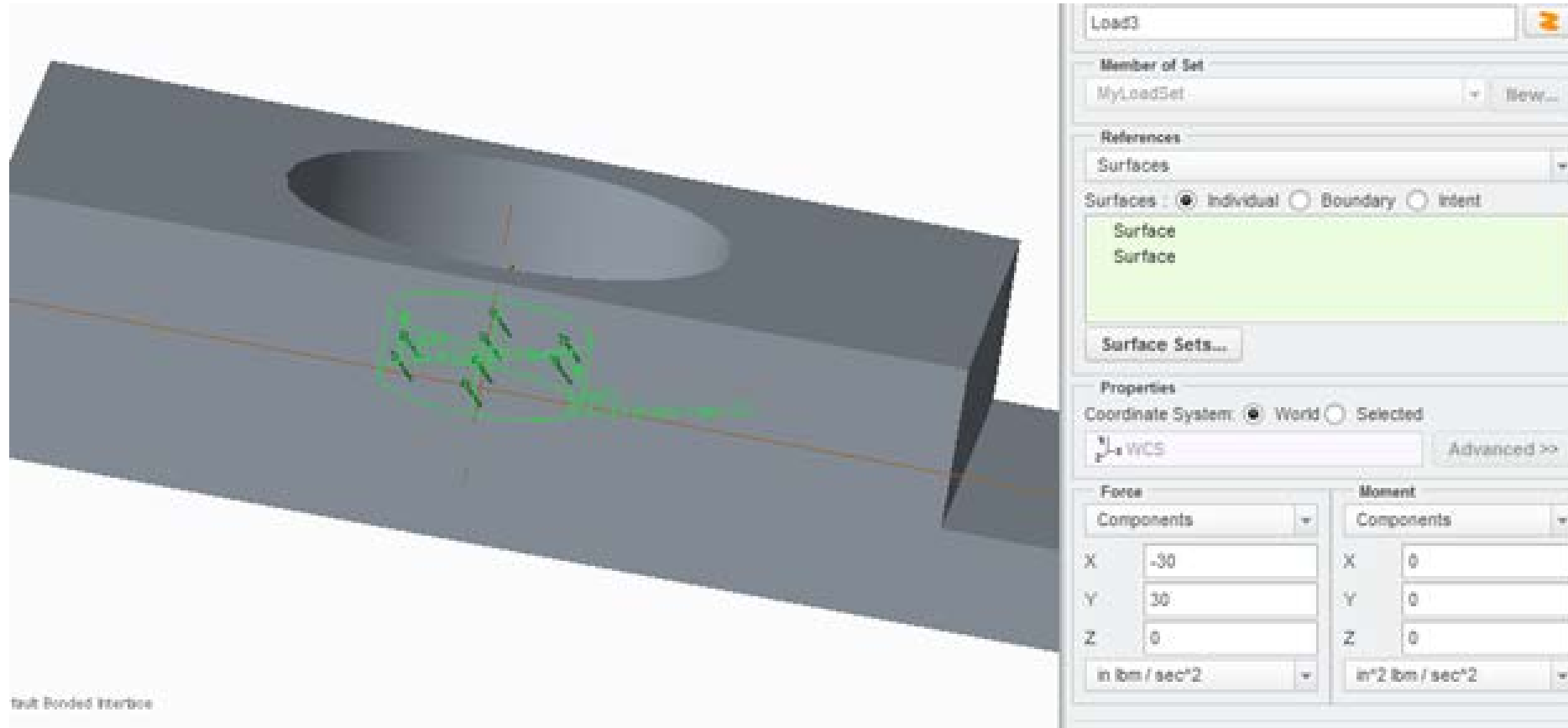


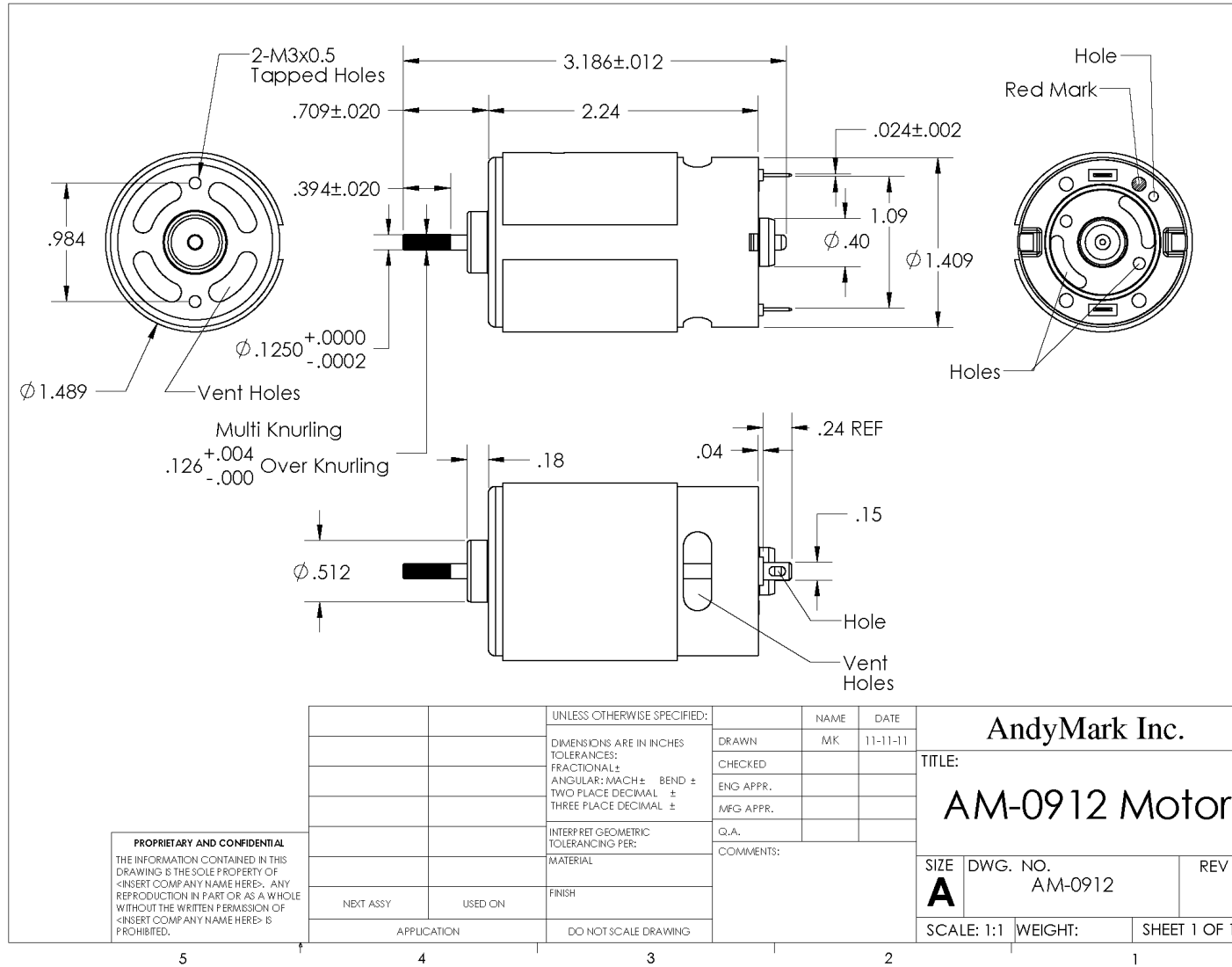
Appendix to Follow

5 psi in the "Y" direction (weight of bracket)



30 psi in the X and Y direction (wind force)





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		UNLESS OTHERWISE SPECIFIED:		NAME	DATE	AndyMark Inc.	
		DIMENSIONS ARE IN INCHES	DRAWN	MK	11-11-11	TITLE:	
		TOLERANCES:	CHECKED			AM-0912 Motor	
		FRACTIONAL ±	ENG APPR.			SIZE	DWG. NO.
		ANGULAR: MACH ± BEND ±	MFG APPR.			A	AM-0912
		TWO PLACE DECIMAL ±	Q.A.				REV
		THREE PLACE DECIMAL ±	COMMENTS:				
		INTERPRET GEOMETRIC TOLERANCING PER:				SCALE: 1:1	WEIGHT:
		MATERIAL					SHEET 1 OF 1
		FINISH					
NEXT ASSY	USED ON						
		APPLICATION	DO NOT SCALE DRAWING				

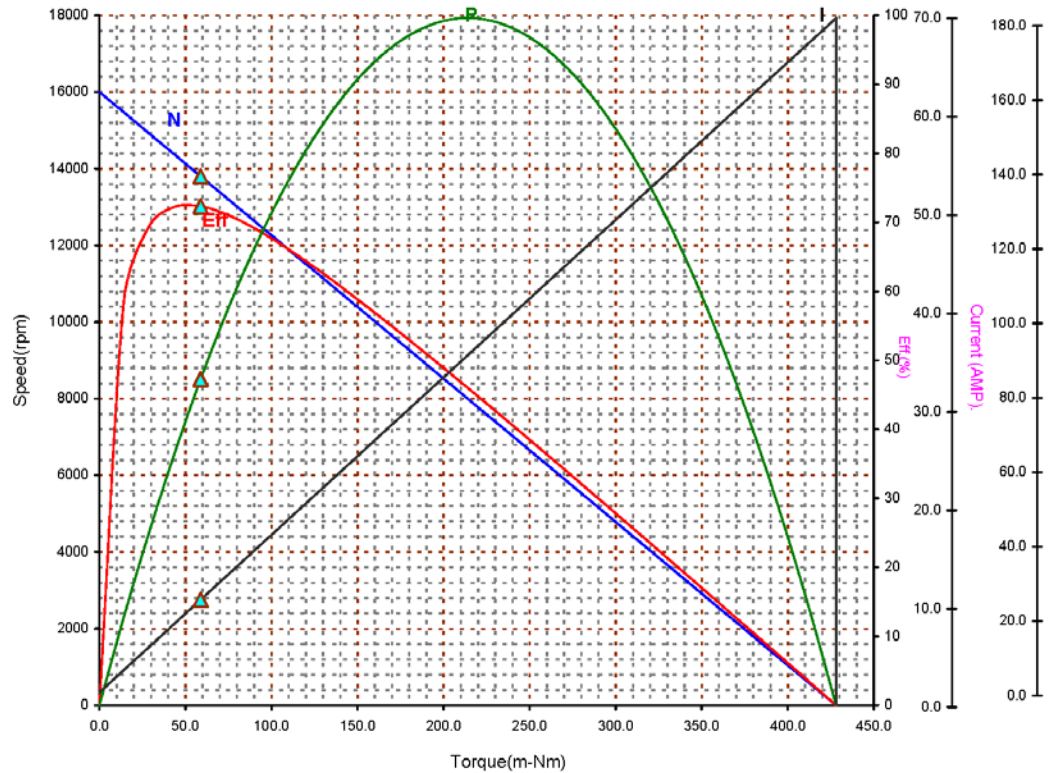
5 4 3 2 1

Chiaphua Components
Group of Companies

<http://www.cclmotors.com>

Project No : DB-30F-2005
 Proposal No:
 Winding : 0.00 - 0
 Motor test reference no : (CCW)

Operator : JACKY
 Date : 2011/11/10



Performance (In an ambient temperature of 25 -30 C)
 Motor tested rapidly to prevent significant temperature rise.

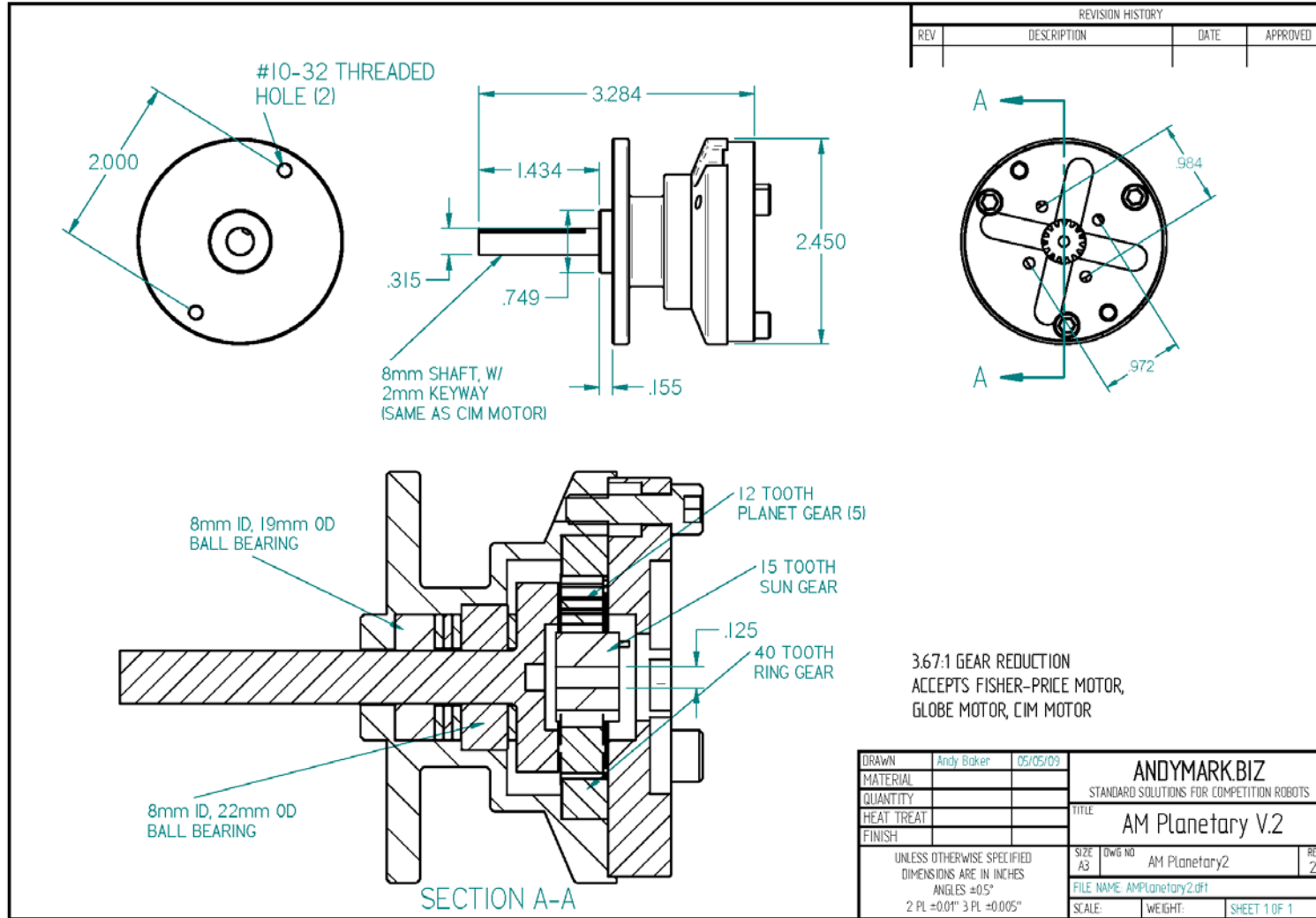
At a constant voltage of 12.00 Volts
 With a circuit resistance 0.000 Ohms

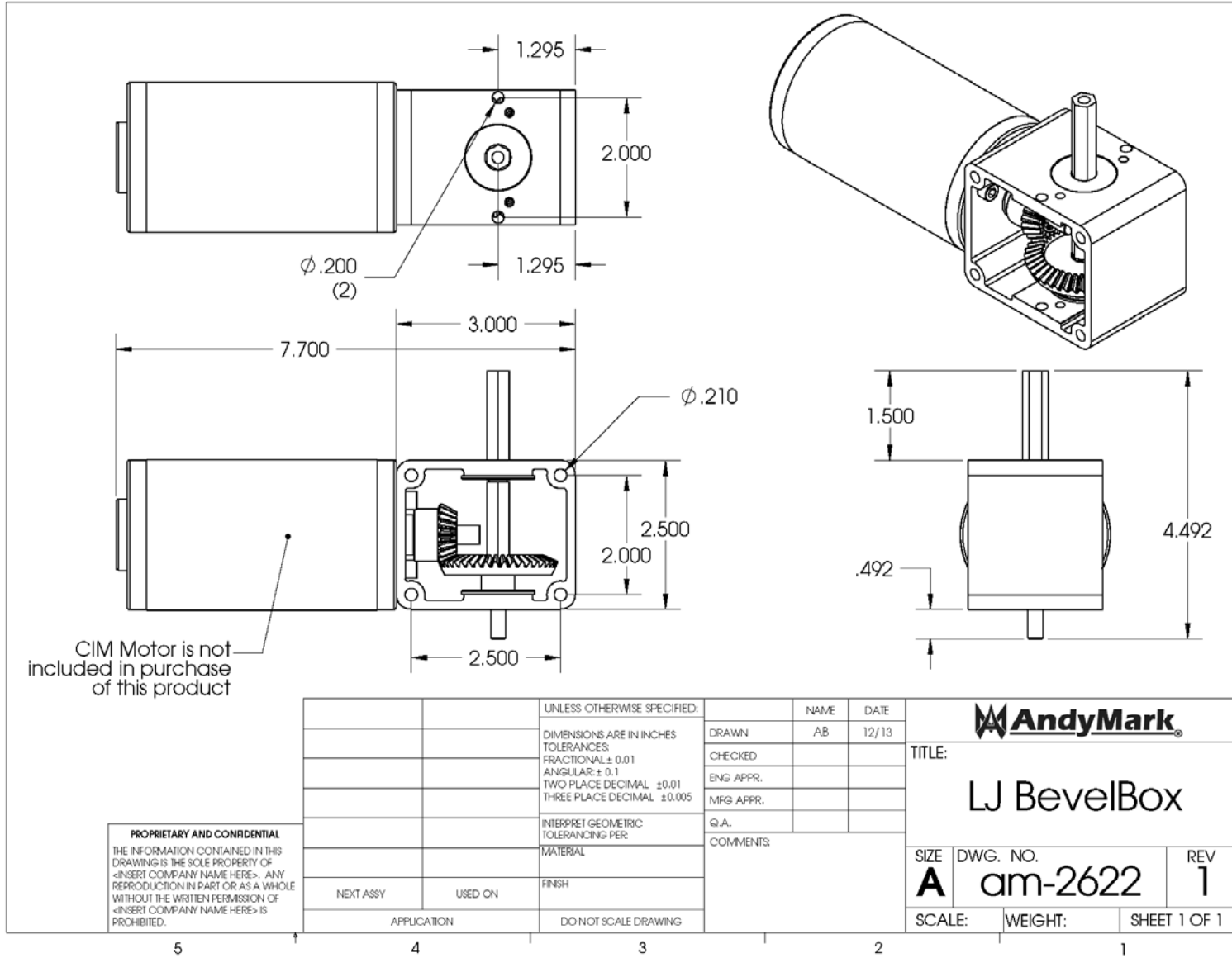
AT No Load	
Speed :	16000 Rpm
Current :	1.200 Amp
At stall (Extrapolated)	
Torque :	428.073 m-Nm
Current :	63.745 Amp
At maximum efficiency	
Efficiency :	72.50 %
Torque :	51.647 m-Nm
Speed :	14070 Rpm
Current :	8.746 Amp
Output :	76.095 Watts
At maximum power	
Torque :	214.036 m-Nm
Speed :	8000 Rpm
Current :	32.473 Amp
Output :	179.311 Watts

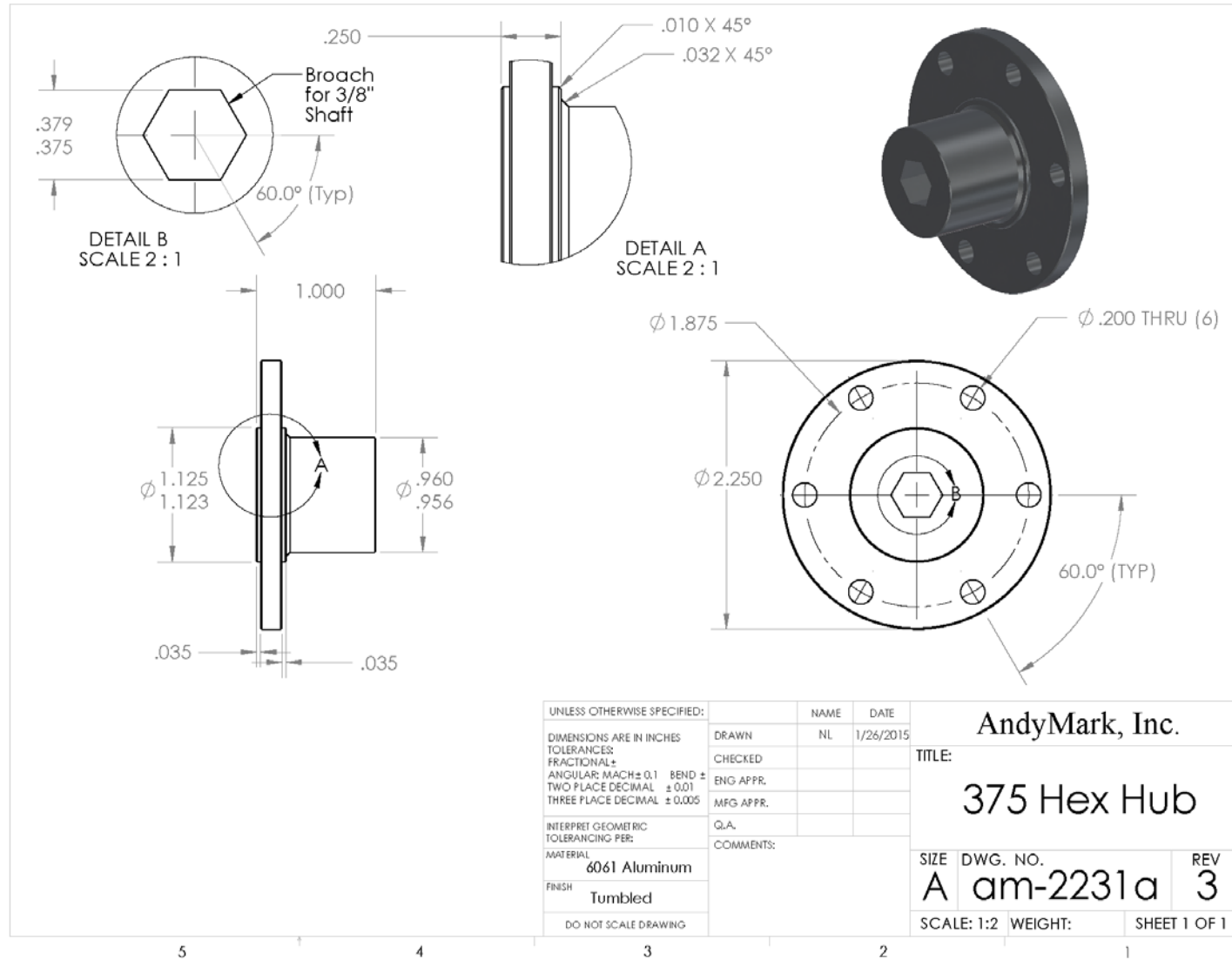
Characteristics	
Torque Constant :	6.844 m-Nm/Amp
E.M.F Constant :	6.844 mV/rad/sec
Dy. Resistance :	0.188 Ohms
Motor Regulation:	37.377 Rpm/m-Nm

Calculation			
At Torque Level:		At Fan:	
Torque:	58.860 m-Nm	Torque:	m-Nm
Speed:	13800 Rpm	Speed:	Rpm
Current:	9.800 Amp	Current:	Amp
Efficiency:	72.33 %	Efficiency:	%
Output:	85.061 Watts	Output:	Watts

COMPUTER PRINT-OUT
 NORMAL MOTOR CURVE
 Performance and characteristics are
 measured based on limited motor
 sample only







Online Metals Purchase Order Form

Vender Information

Name: Online Metals

Item Description	Item Number	Qty*	Price	Total Cost
Aluminum 6061T651 Plate 0.3125" Cut to: 1.75" x 18"		1	12.92	12.92
Aluminum 6061T651 Plate 0.375" Cut to: 7.25" x 3.25"		1	8.01	8.01
Aluminum 6061T651Plate 0.25"Cut to: 4" x 15"		3	13.20	41.1
Aluminum 6061T651Plate 0.5"Cut to: 1" x 1"		6	0.45	8.7
Aluminum 6061T6Sheet PVC 1 side 0.125"Cut to: 16.25" x 5.25"		4	13.65	57.6
Aluminum 6061T6Sheet PVC 1 side0.125"Cut to: 5" x 3"		3	2.4	8.7
Aluminum 6061T651BarePlate 0.25"Cut to: 9" x 8"		1	15.84	15.84

SUB TOTAL: 152.87

McMaster-Carr Purchase Order Form

Vender Information

Name: McMaster

Item Description	Item Number	Qty*	Price	Total Cost
Push/Pull Action Toggle Clamp, Hole Mounted, 200 lb Maximum Holding Capacity, 3-1/8" Height	5093A56	2	16.51	33.02
Replacement Holding Screw for Toggle Clamp, Nonmarring Flat-Tipped, 1/4"-20x 1-5/8" Screw Size, Steel	5147A63	2	3.34	6.68
Permanently Lubricated Ball Bearing	2342K187	1	20.66	20.66

SUB TOTAL: 60.36






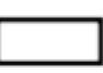



AndyMark Purchase Order Form

Vender Information

Name: AndyMark, Inc

Item Description	Item Number	Qty*	Price	Total Cost
AM Planetary Single Stage	Am-2491	1	45.00	45.00
AM Planetary Gearbox, 3 Stage, 49.4:1 Ratio	am-2547	1	180.00	180.00
Sun Gear, 15 Tooth, 32 dp	am-0040	1	9.00	9.00
LJ Bevel Box with 3/8 Hex Output Shaft	am-2622	1	129.00	129.00
Encoder Mount Pad	am-0208	1	4.00	4.00
E4T OEM Miniature Optical Encoder Kit	am-3132	1	42.00	42.00
FR6ZZL-hex Bearing	am-0692	1	5.00	5.00
1/4-20 x 5/8" SHCS [Qty-10]	am-1203	1	2.00	2.00
AndyMark 9015 Motor	am-0912	1	14.00	14.00

SUB TOTAL: 430.00

Shape	Drag Coefficient
Sphere → 	0.47
Half-sphere → 	0.42
Cone → 	0.50
Cube → 	1.05
Angled Cube → 	0.80
Long Cylinder → 	0.82
Short Cylinder → 	1.15
Streamlined Body → 	0.04
Streamlined Half-body → 	0.09

Measured Drag Coefficients

Drag coefficients in fluids with Reynolds number approximately 10^4

all other targets can be assessed from largest target (fig 11)

$$A_2 := 17.25\text{in} \cdot 45\text{in} = 0.501\text{m}^2$$

$$C_{d2} := 0.82$$

$$F_{d2} := 0.5 \cdot \rho \cdot v^2 \cdot A_2 \cdot C_{d2} = 13.843\text{ lbf}$$

$$F_{m2} := F_{d2} \cdot 22.5\text{in} = 25.956\text{ lbf} \cdot \text{ft}$$

NATO Style Figure 11 Target

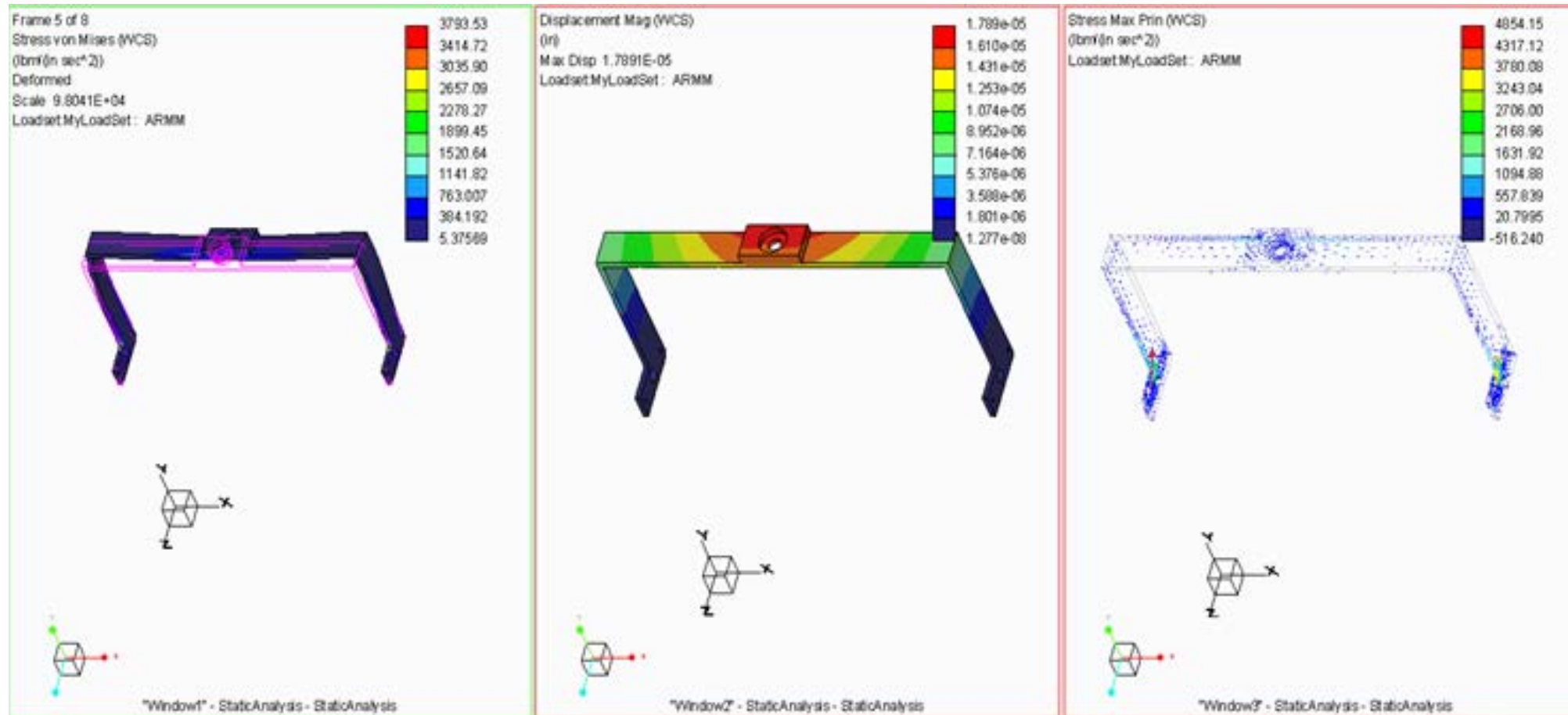


It can be assumed the largest force felt is $50\text{ lbf} \cdot \text{ft}$
 $50\text{ lbf} \cdot \text{ft} = 67.791\text{ N} \cdot \text{m}$

Since the student edition cant do moments i am substuting it as a force by deviding by the parameter

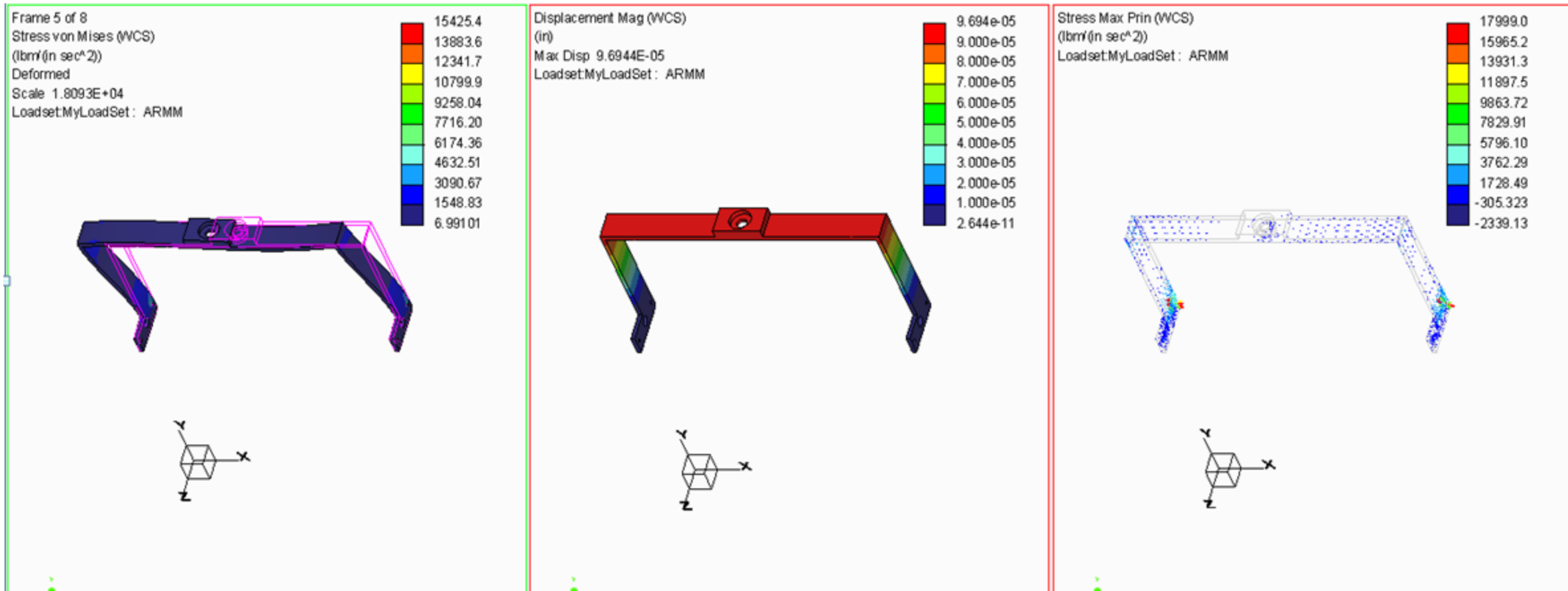
$$\frac{(50\text{ lbf} \cdot \text{ft})}{\pi \cdot 0.5\text{in}} = 381.972\text{ lbf}$$

Appendix

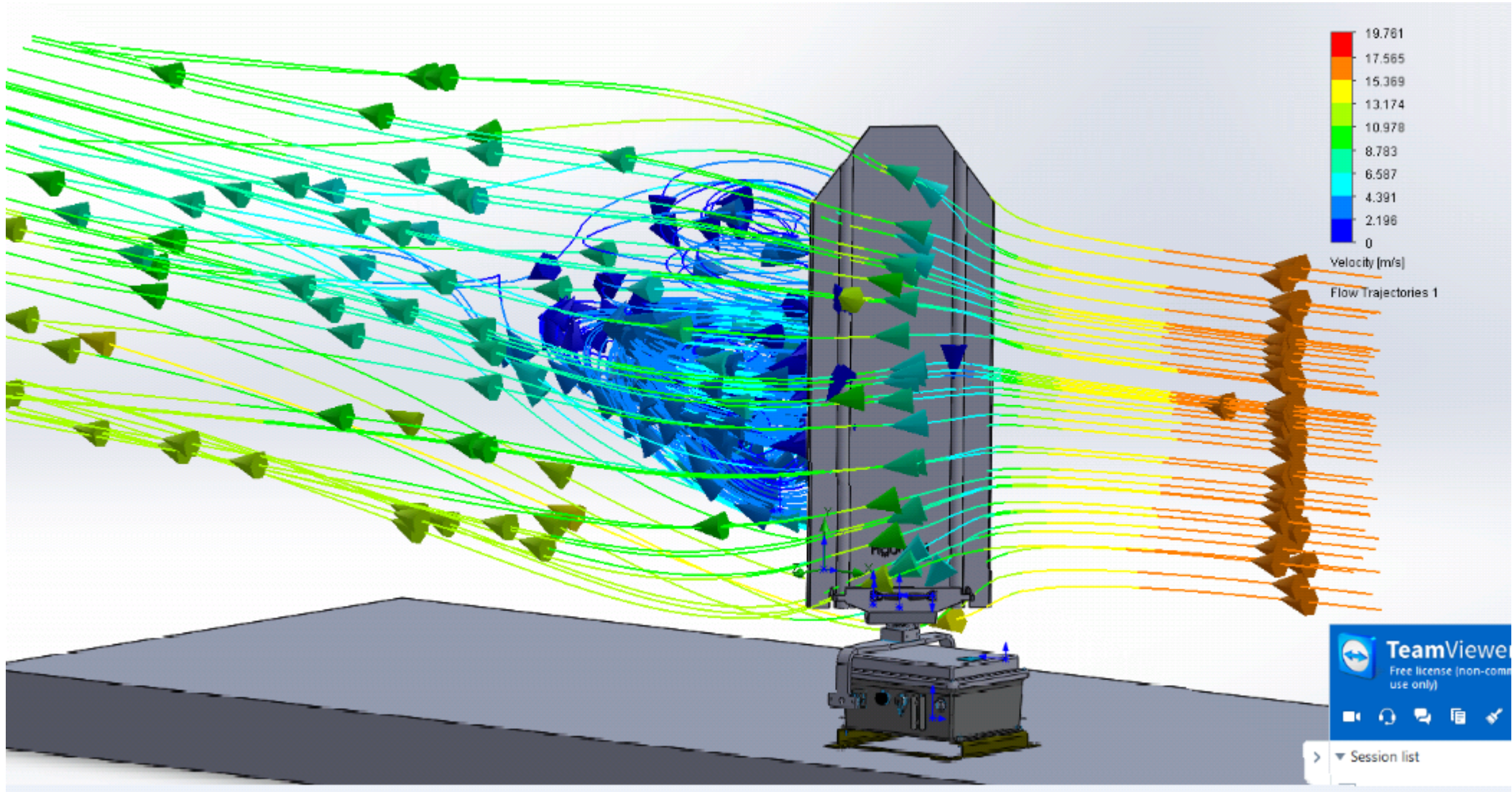


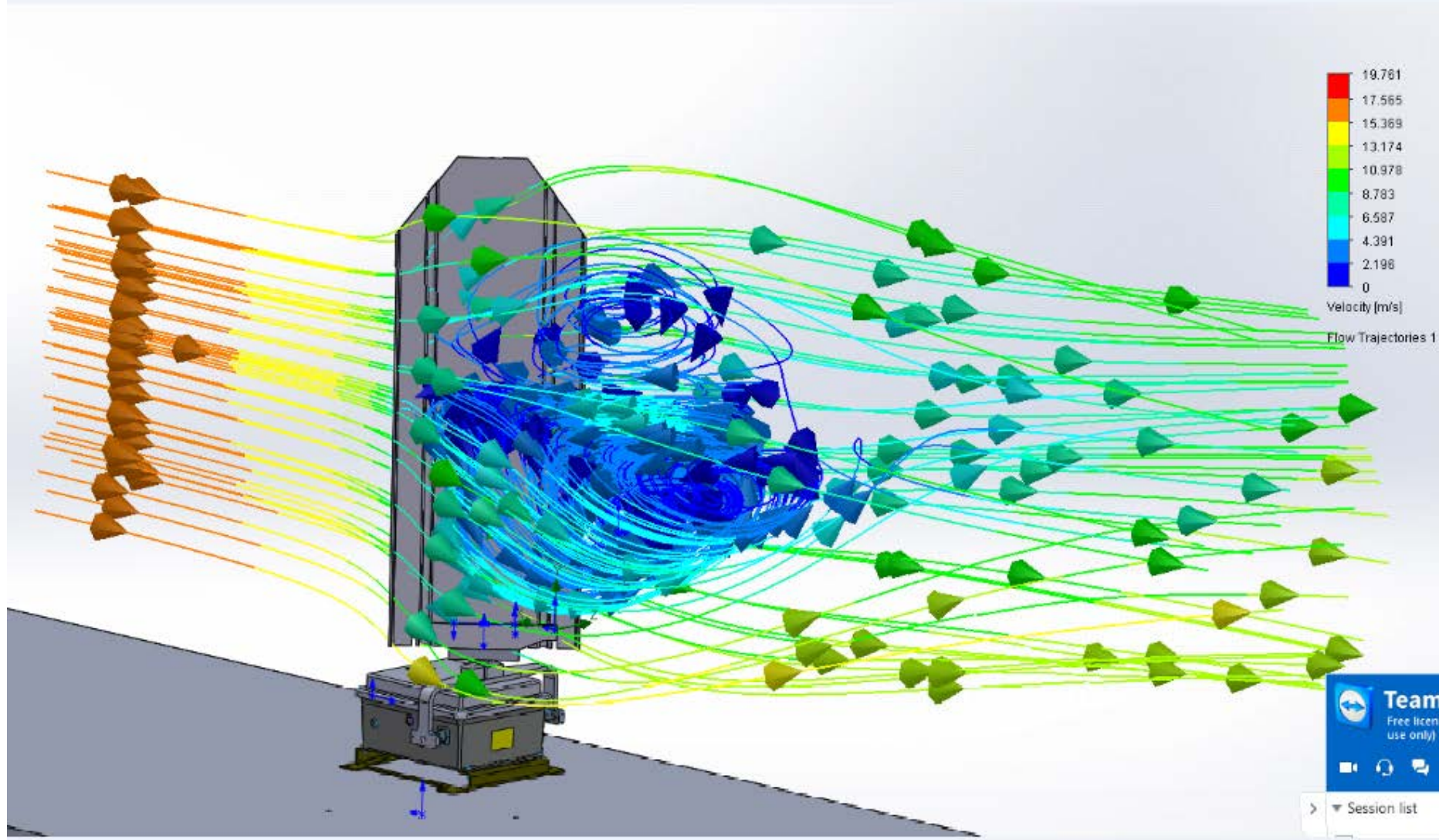
- Applied force only in the “Z” Direction

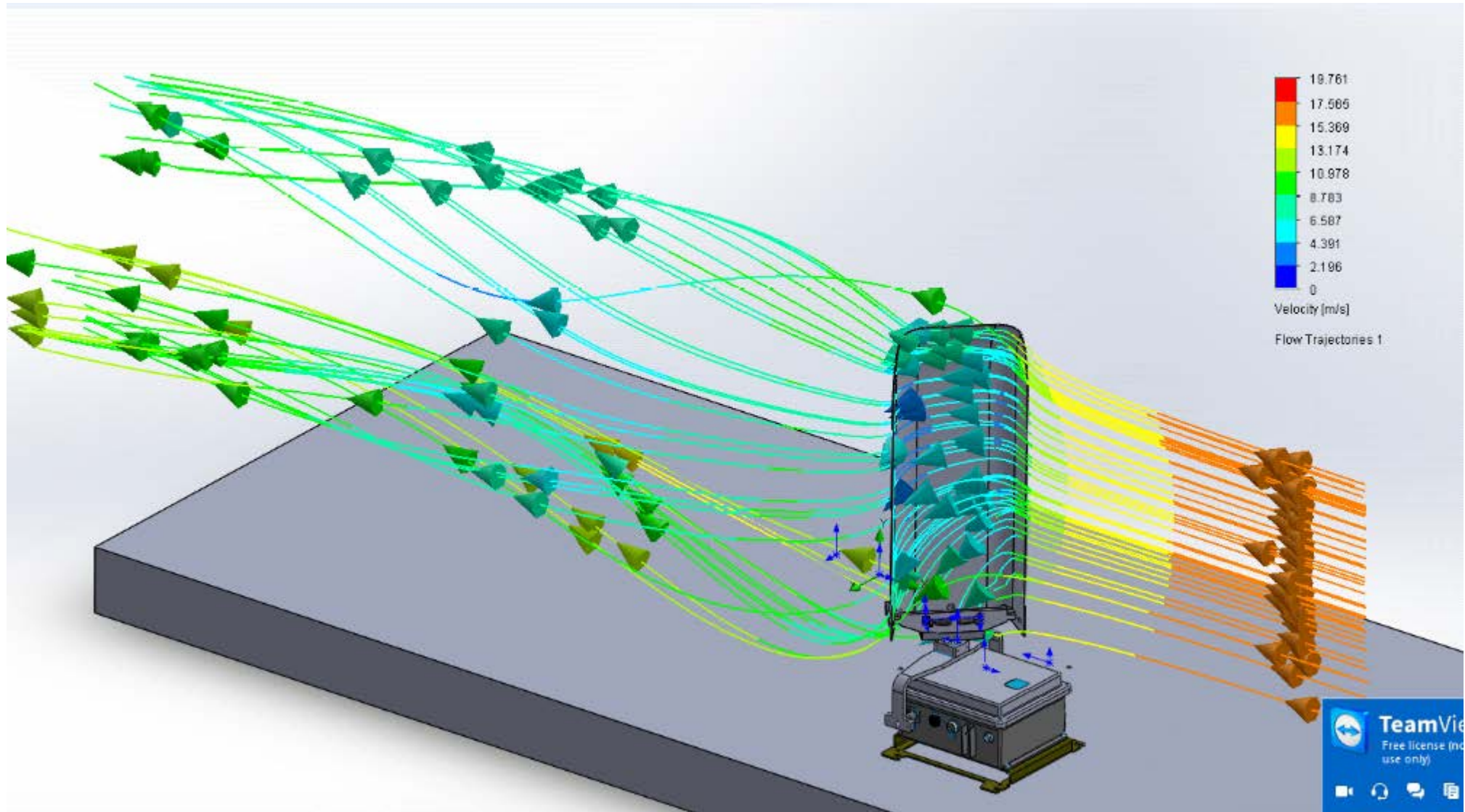
Appendix

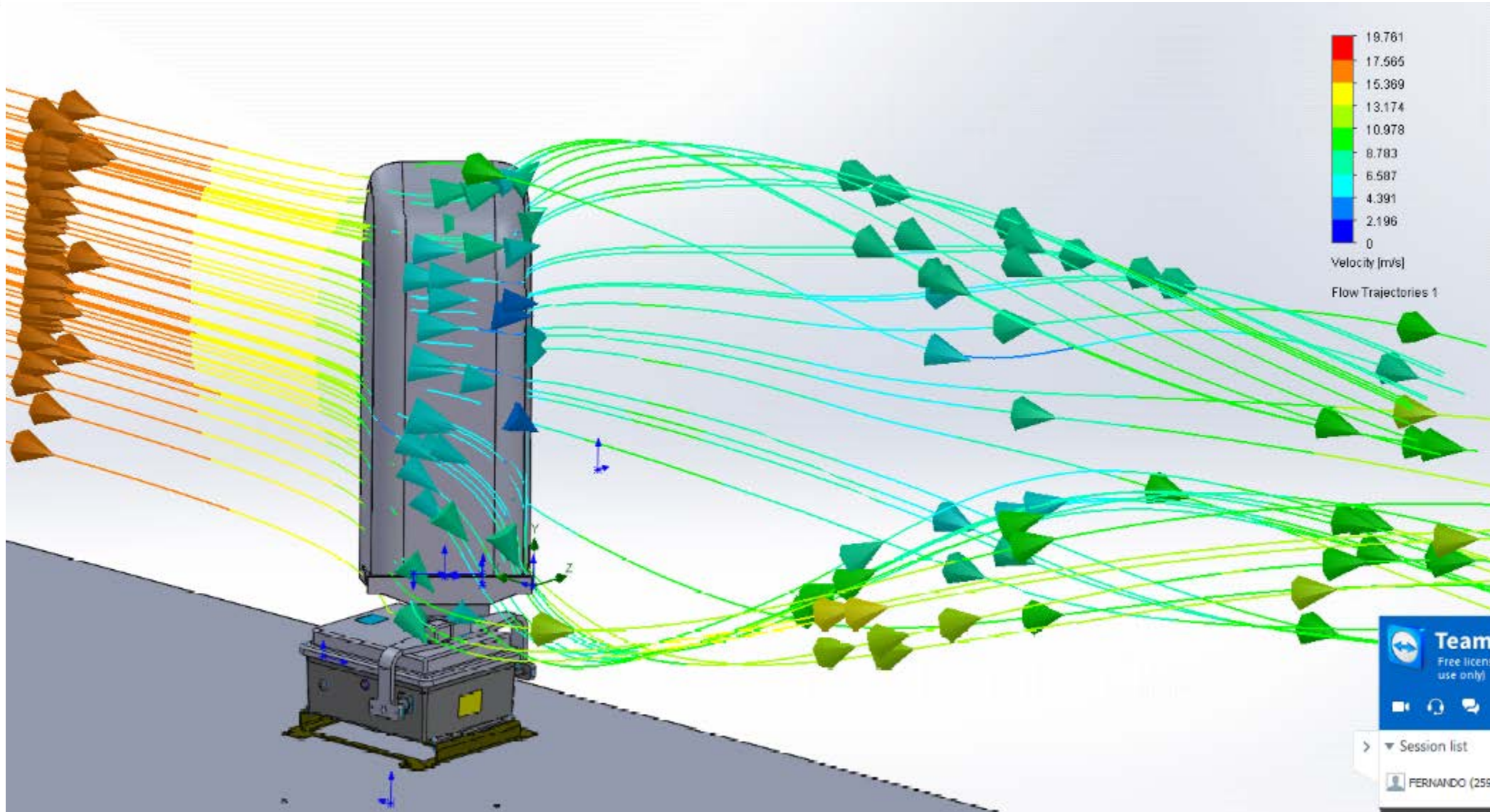


- Applied force only in the “x” Direction (not designed for)









Design Analysis

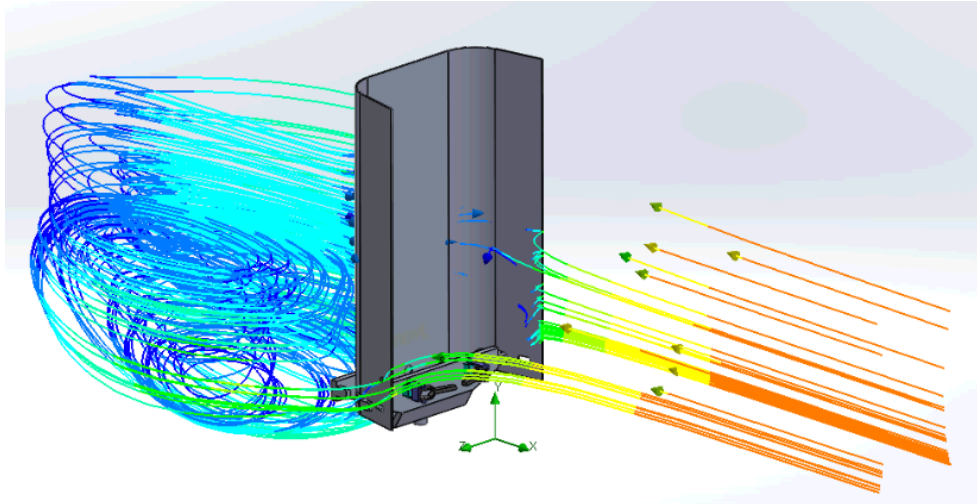


Fig. 17

$$\rho := 1.225 \frac{\text{kg}}{\text{m}^3}$$

Density of Air

$$v := 35 \text{ mph}$$

Velocity of Wind

$$A := \pi \cdot 6 \text{ in} \cdot 3 \text{ ft} = 4.712 \text{ ft}^2$$

Area of Ivan

$$C_d := 1.45$$

Drag coefficient of Ivan

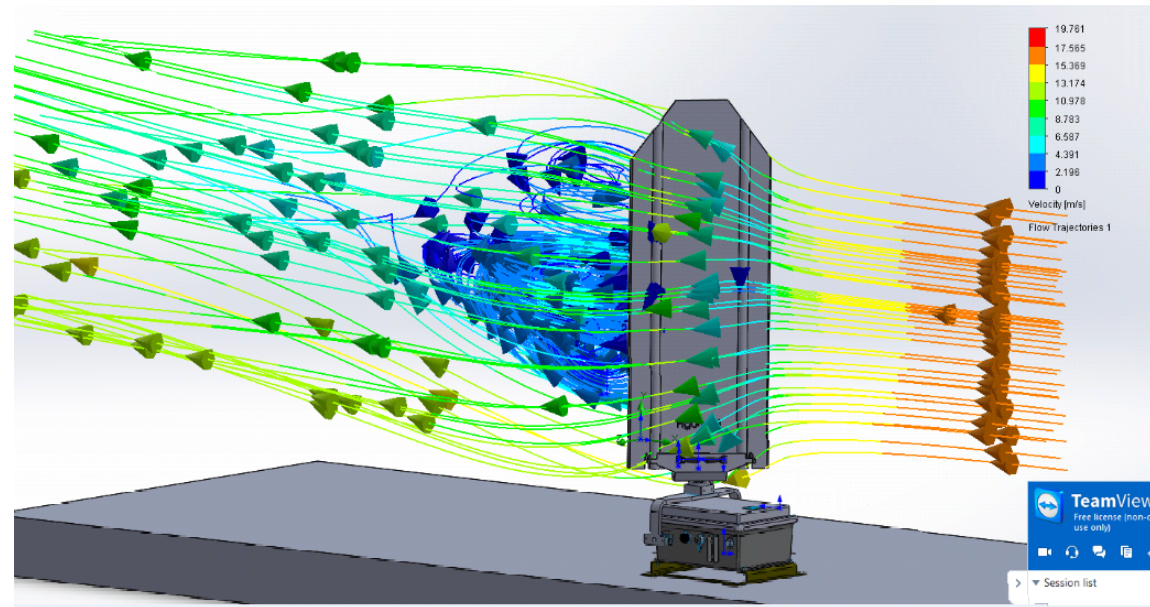
$$F_d := 0.5 \rho \cdot v^2 \cdot A \cdot C_d = 21.399 \text{ lbf}$$

Resultant Force

- Worst case scenario: 35 mph wind blowing on the back of the Ivan

Design Analysis

- Max torque generated from the distributed wind force = **11.5 ft*lbf (15.592N*m)**
- Our bracket currently secures each of these targets with two clamps each rated for 100 lbf



all other targets can be assessed from largest target (fig 11)

Fig. 18



CFD Simulation for Wind

- Solidworks was used to provide a basic simulation of gust winds on target
- This was done to achieve reliable numbers to base motor specs and structural analyses on
- The simulation was done for both the Ivan target and the biggest flat type target
- Simulation was run multiple times for the multiple angles the wind could be blowing on the target

CFD Simulation for Wind

- The maximum torque on the motor due to wind was 11.5 ft*lbfs
 - Generated on Ivan with wind attacking at 135 degrees (Fig. 26)
- The maximum forces seen on any target was 21.3 lbfs
 - Generated on flat target with angle of wind straight on (Fig. 27)

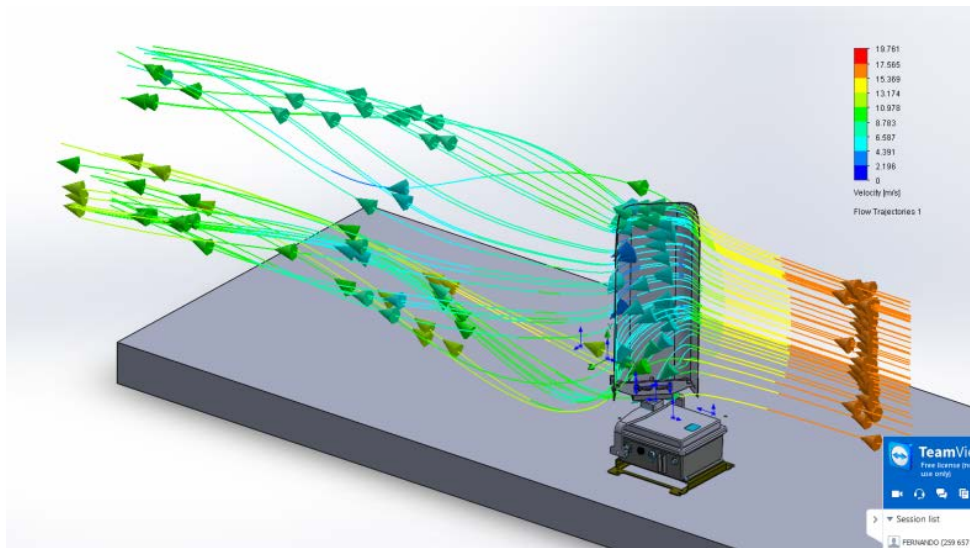


Fig. 26

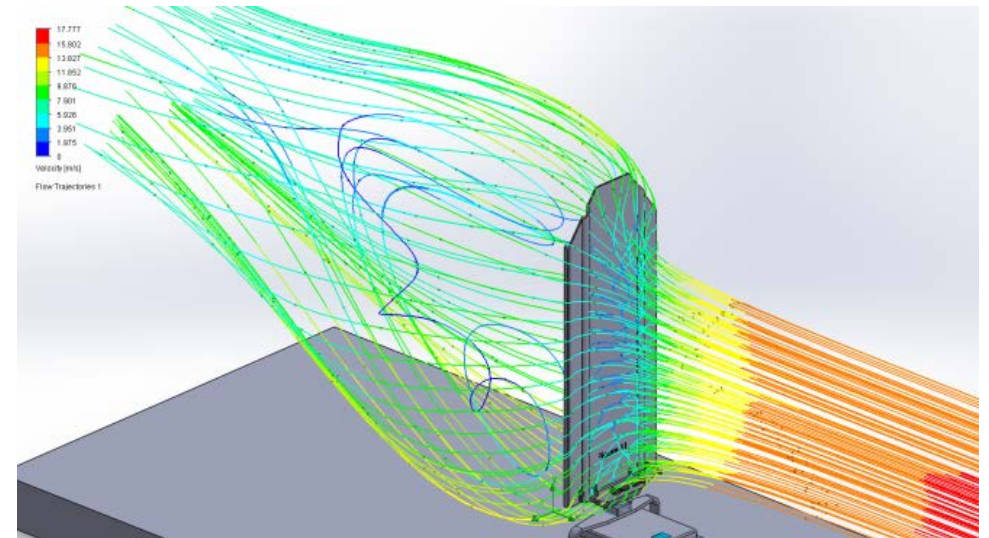


Fig. 27

Motor Selection



CCL-9015 12VDC Brushed Motor

Fig. 28

- Length: 3.19 inches
- Weight: 0.5 pounds
- At max power of 179.3W:
 - 32.5 amps
 - **Torque: 30.32 oz-in**
 - 8000 RPM

Gearing Selection

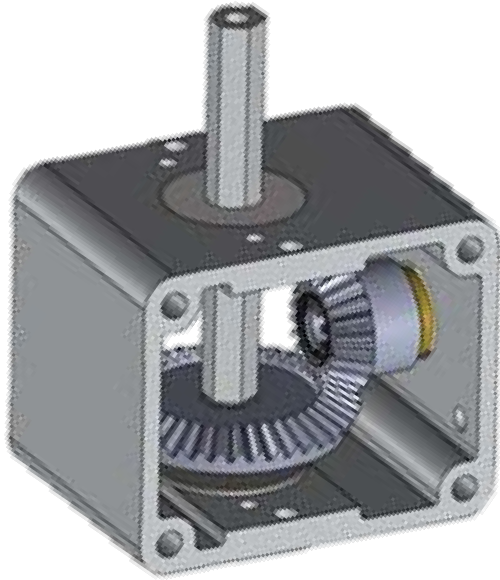


AM-0002 Planetary Gearbox

Fig. 29

- Length: 2.5 inches
- Weight: 0.63 pounds
- Reduction: 3.67:1
 - 2 additional gear stages will be added to help meet the required torque

Gearing Selection

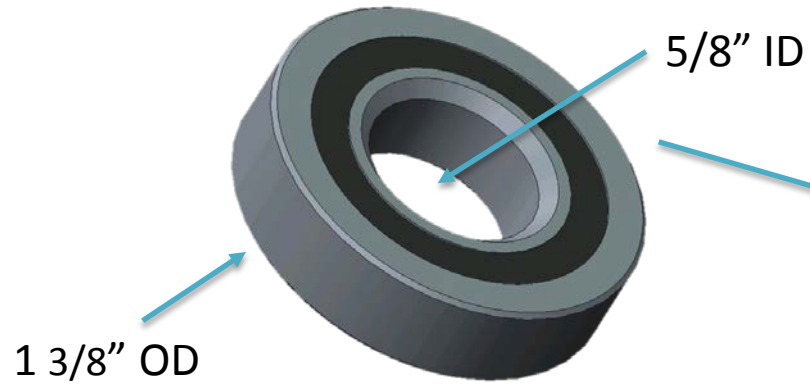


**LJ Bevel Right Angle
Gearbox**

Fig. 30

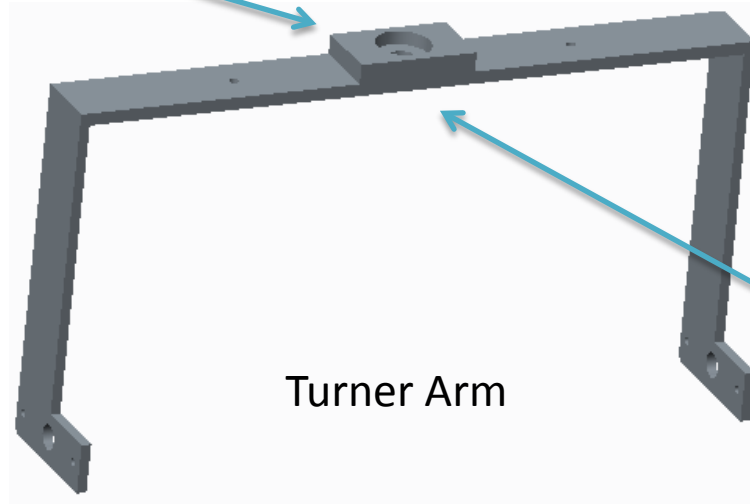
- Dimensions:
3 x 2.5 x 2.25 in
- Weight: 0.95 pounds
- Reduction: 2:1

Bearing Selection



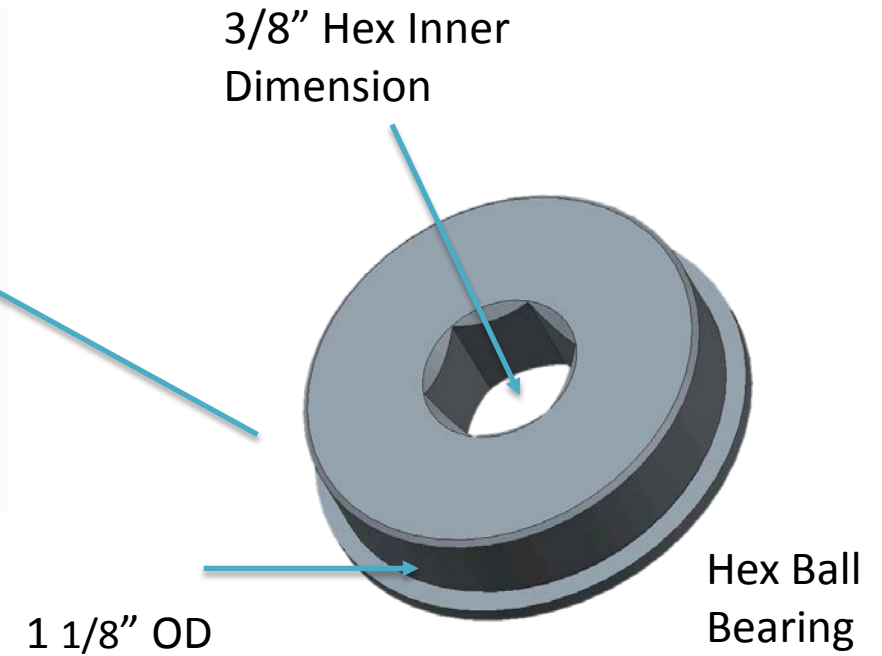
Double Sealed and Permanently Lubricated ball bearing

Fig. 32



Turner Arm

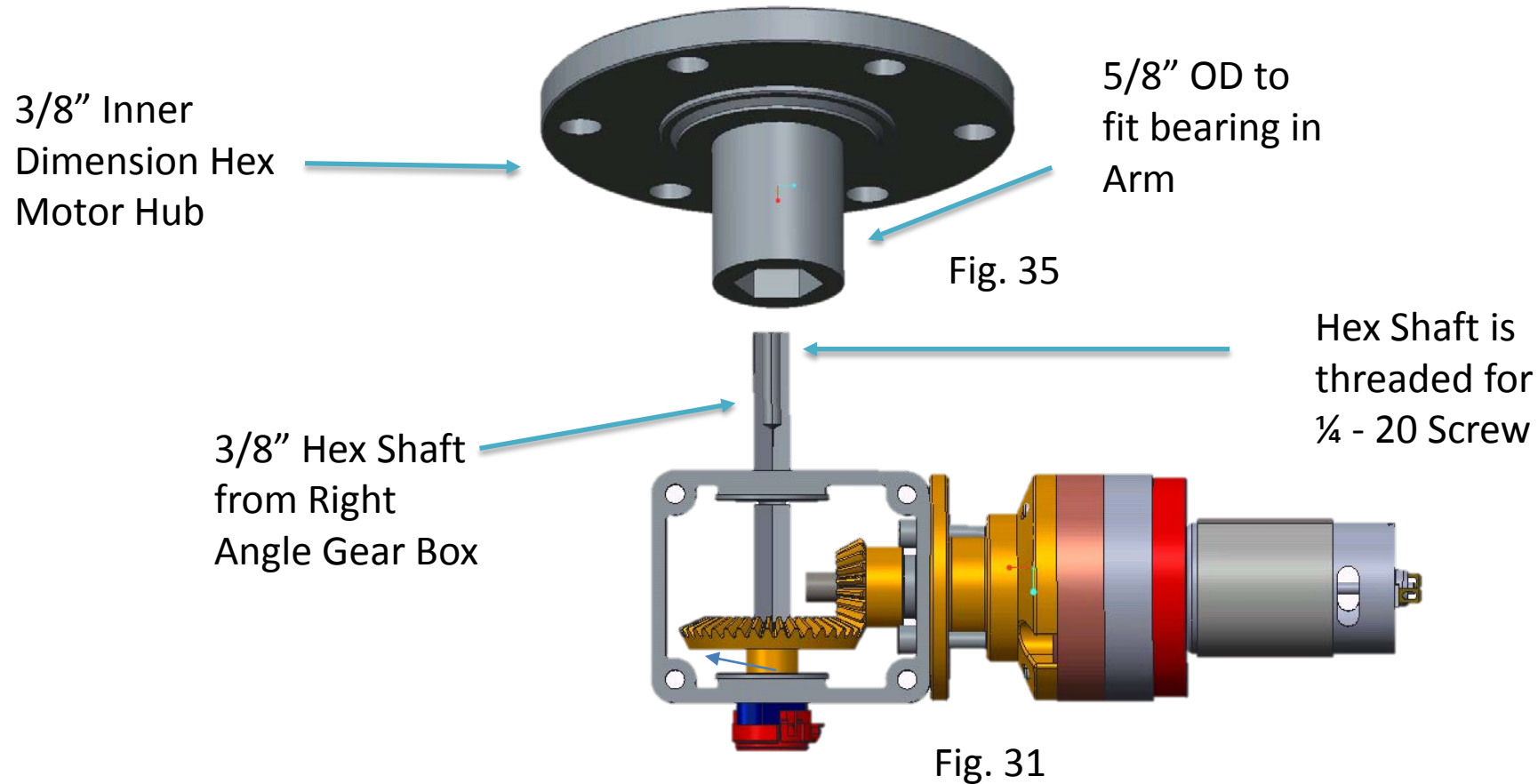
Fig. 33



Hex Ball Bearing

Fig. 34

Turning Mechanism to Bracket Coupling



Appendix

Current Design:



Down Position



Up Position

Appendix

Proposed Design:



Down Position



Up Position
with Rotation

Appendix

- Adding to Lockheed-Martin's current SIT to allowing for rotation of the of the target
- Create a universal bracket for variety of targets
- Produce a functional prototype of our selected design





Design Specifications

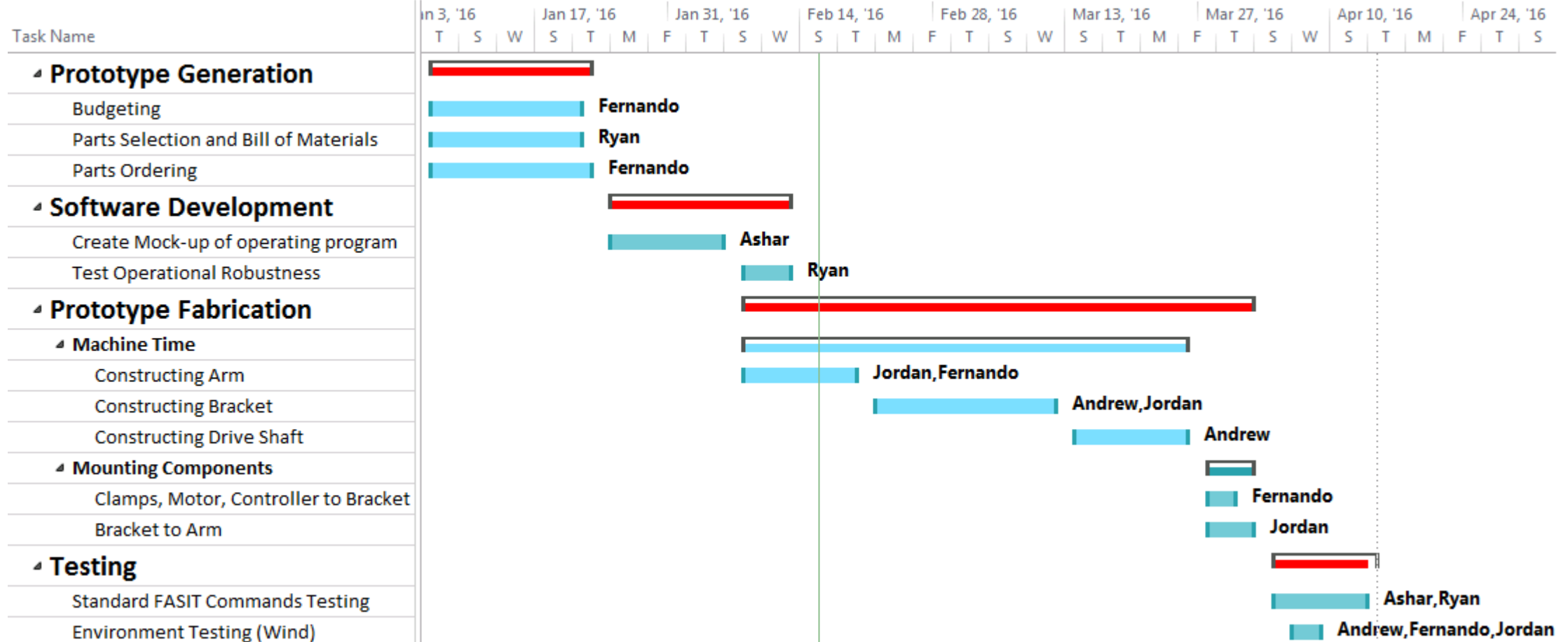
- Time to install new target shall be less than 10 seconds
- Motor housing shall be rated to at least IP67
- Motor shall rotate target 90° in either direction within 1 second of receiving command
- Distance from bottom of lifter to top of the bracket shall be no more than 18"
- Weight of lifter arm with turner motor shall be no more than 10 lbs.
- Arm shall not impede other integrated SIT functionalities
- Firmware shall be compatible with all FASIT 2.0 commands
- Bracket and arm must be able to hold the target in 35 mph winds
- Combined operational and storage temperature: -20°C to 60°C



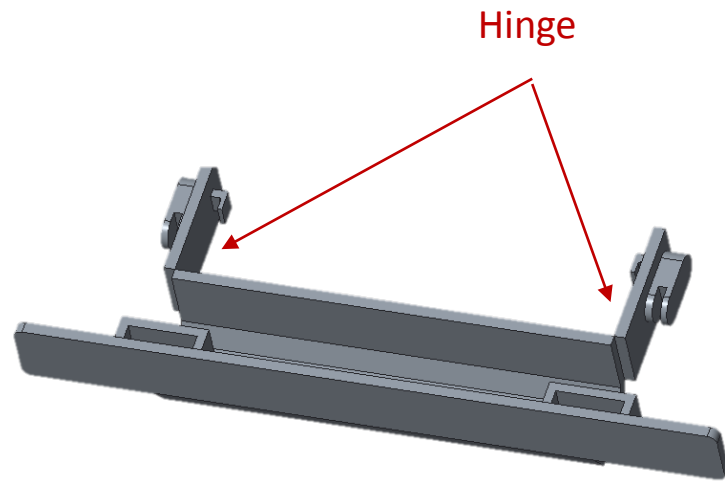


Future Work

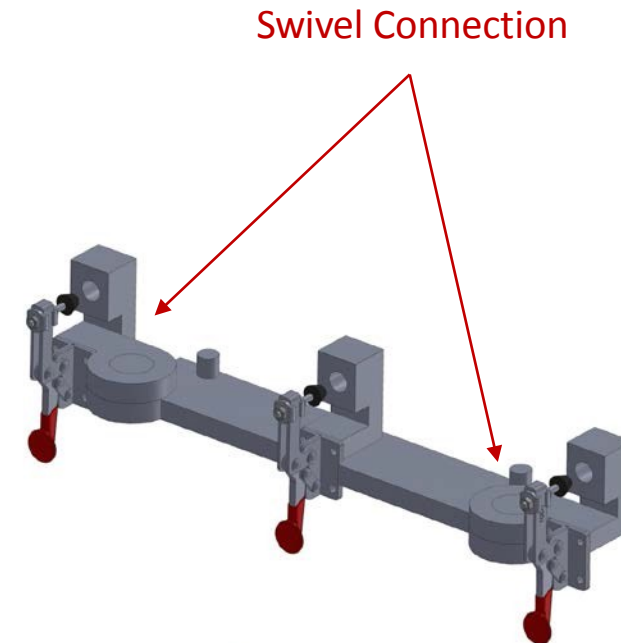
Schedule:



Previous Target Brackets



Example of
Previous Bracket 1



Example of
Previous Bracket 2



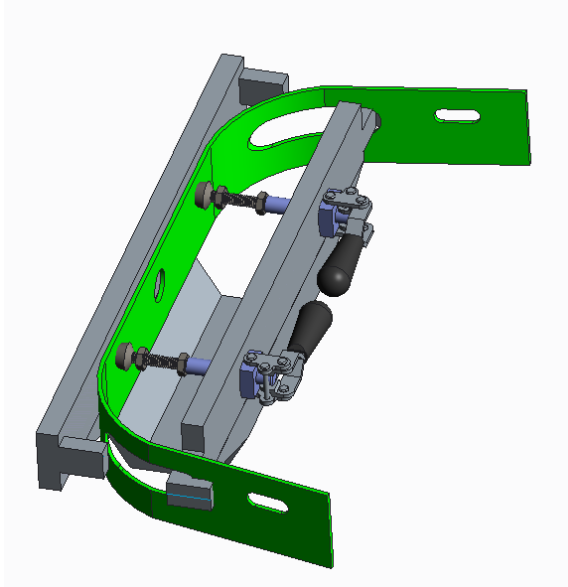
Target Bracket Progress

New Developments:

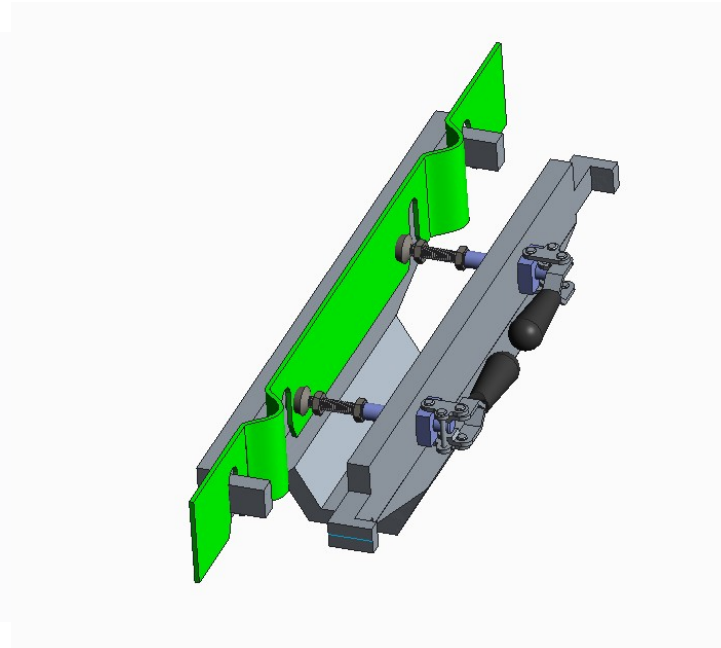
- From sponsor feedback, many of the team's previous designs were inadequate due to various uses of a hinge or other similar moving parts
- Hinges inadequate due to operational conditions, specifically the SIT's environment
- Previous designs were amended to incorporate an alternate form of latching/locking mechanism

Amended Turning Bracket Designs

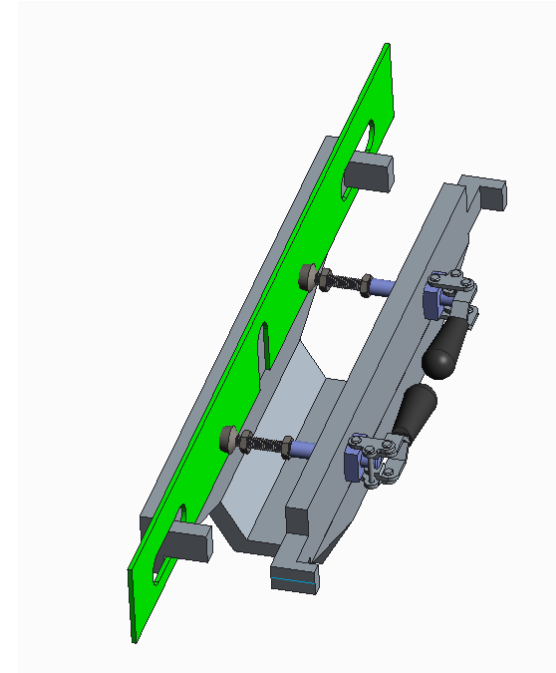
New Bracket Design 1:



“Ivan” Target Fit



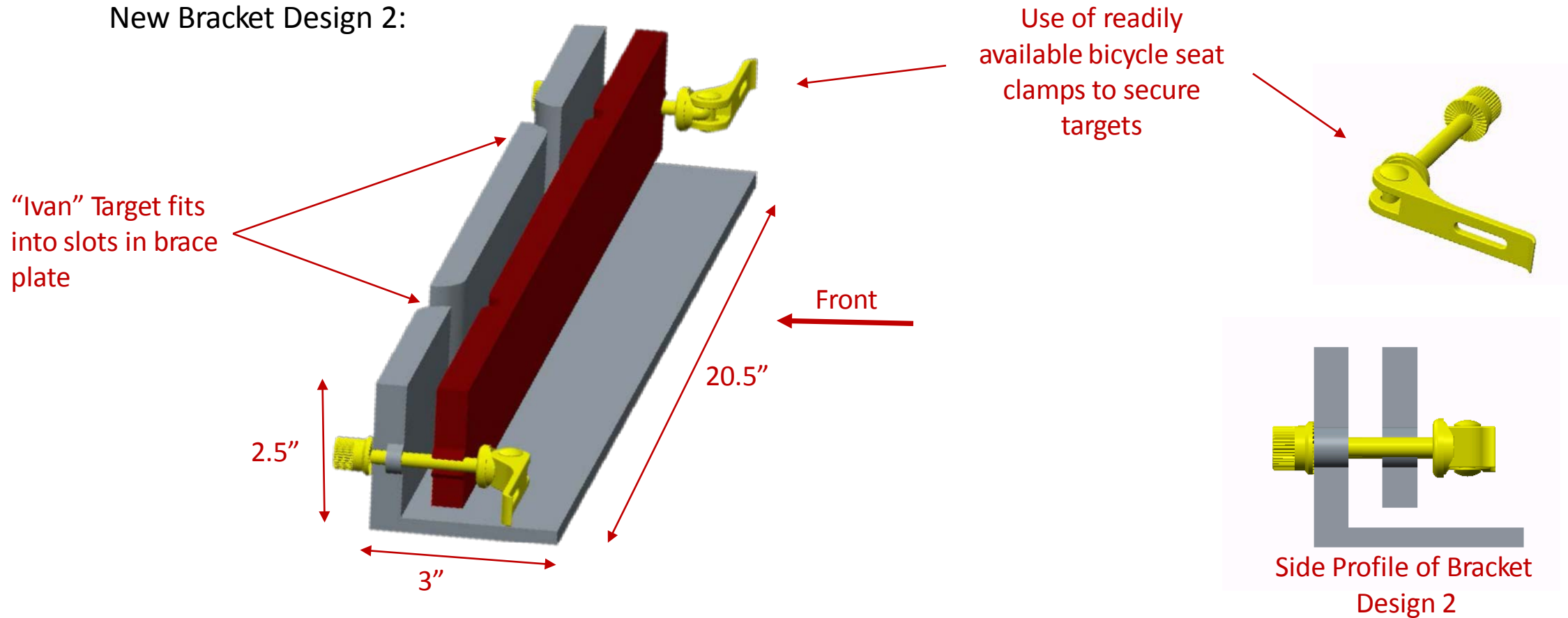
“Figure 11” and “Figure 12” Target Fit



“Waffle Board” Target Fit

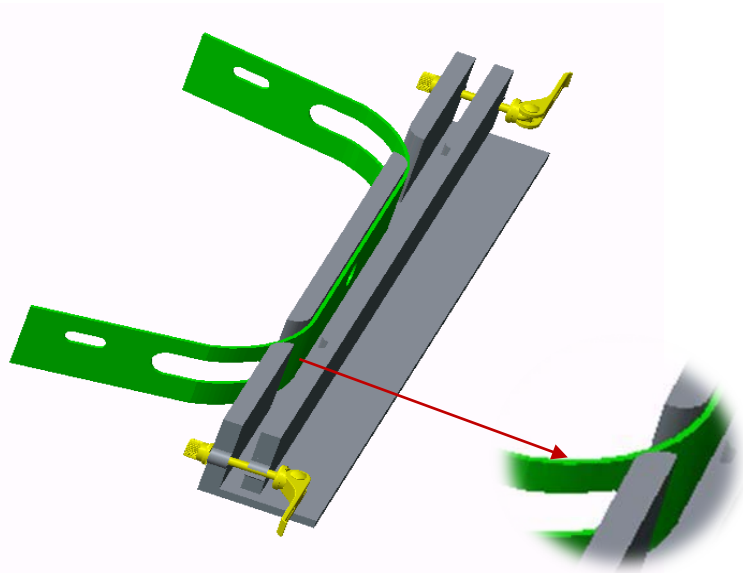
Amended Turning Bracket Designs

New Bracket Design 2:

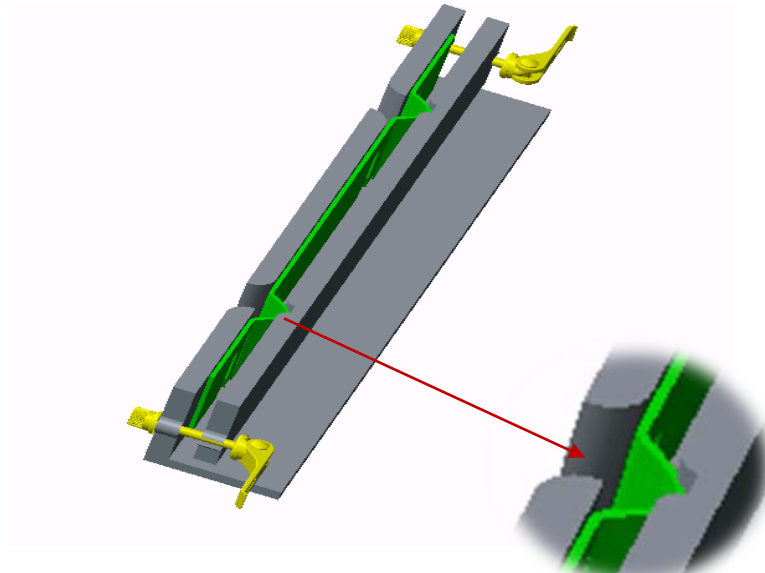


Amended Turning Bracket Designs

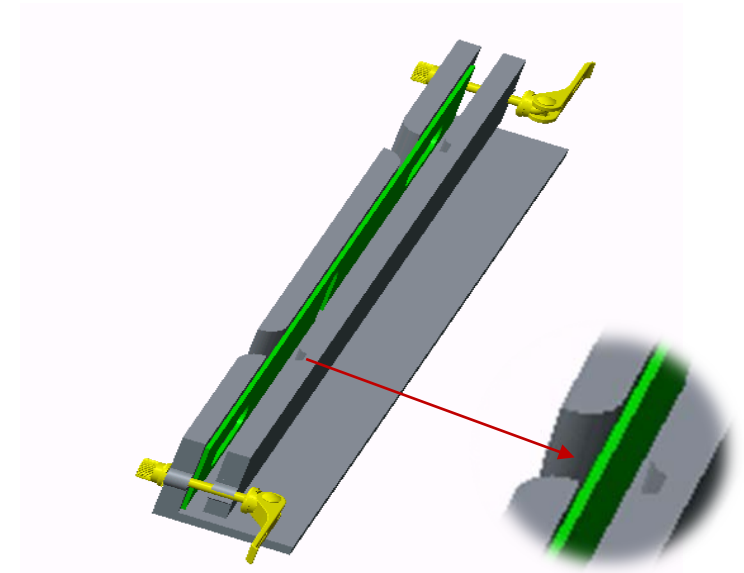
New Bracket Design 2:



“Ivan” Target Fit



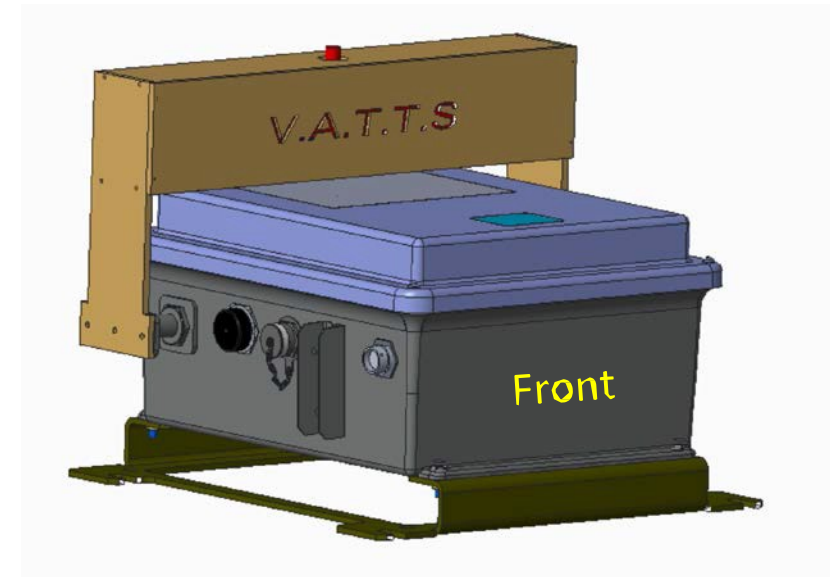
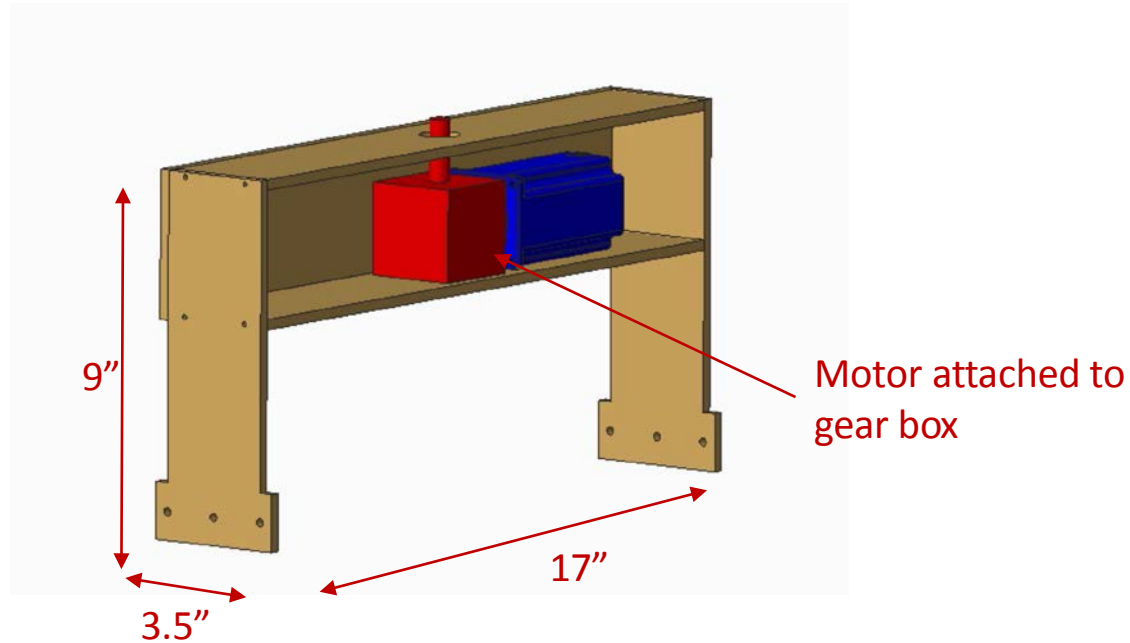
“Figure 11” and “Figure 12” Target Fit



“Waffle Board” Target Fit

Lifting and Turning Arm Designs

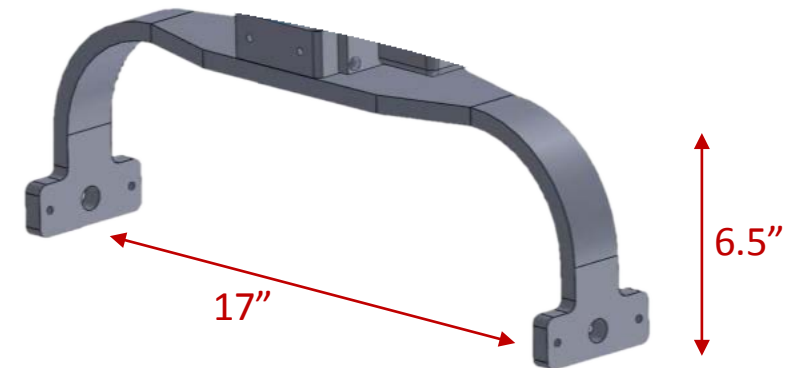
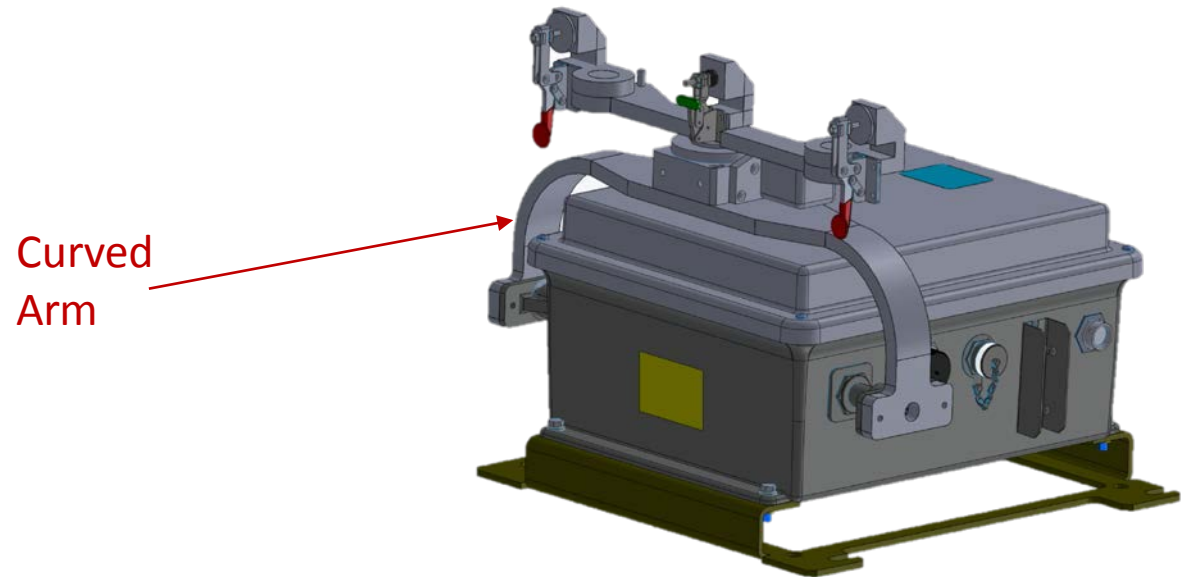
Arm Design 1:



Arm Design Attached to Provided Lifter

Lifting and Turning Arm Designs

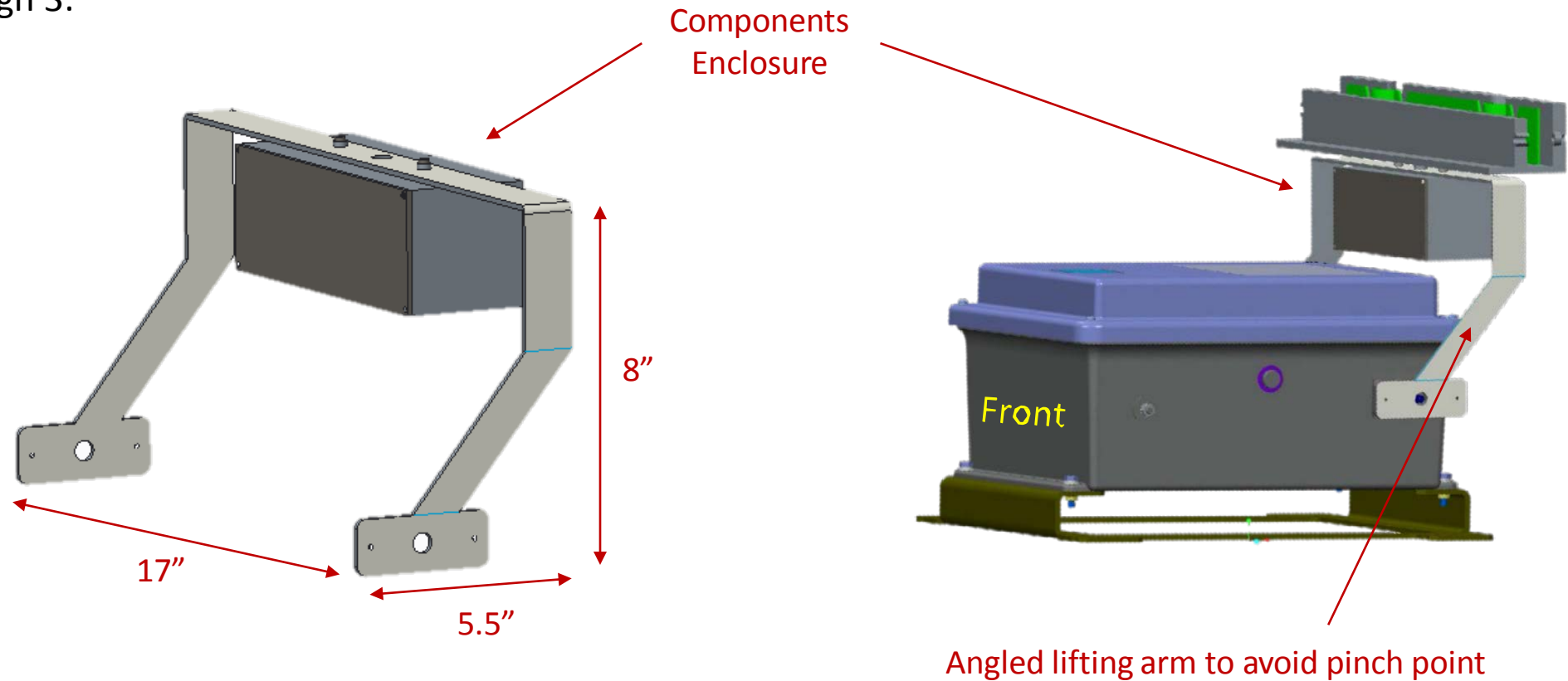
Arm Design 2:





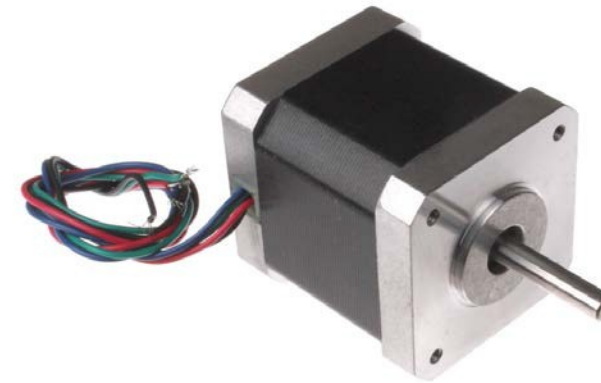
Lifting and Turning Arm Designs

Arm Design 3:



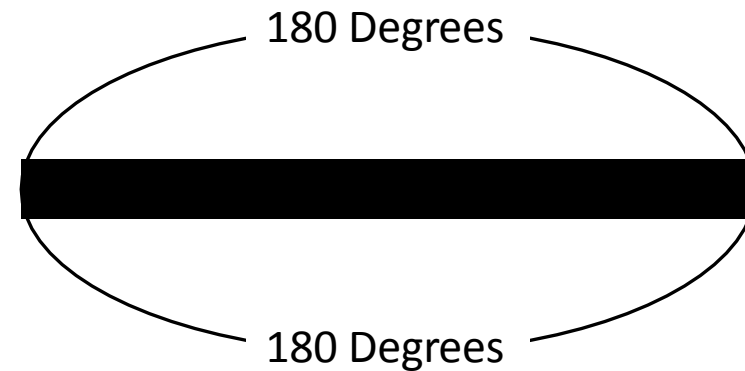
Target Turning Motor Selection

- Stepper Motor
 - Provides a Full Range of Motion
 - Precision Control
 - Open-Loop Feedback
 - High Holding Torque
- Ideal for quick and accurate positioning over short distances
- Team has experience working with stepper motors



Target Turning Motor Selection

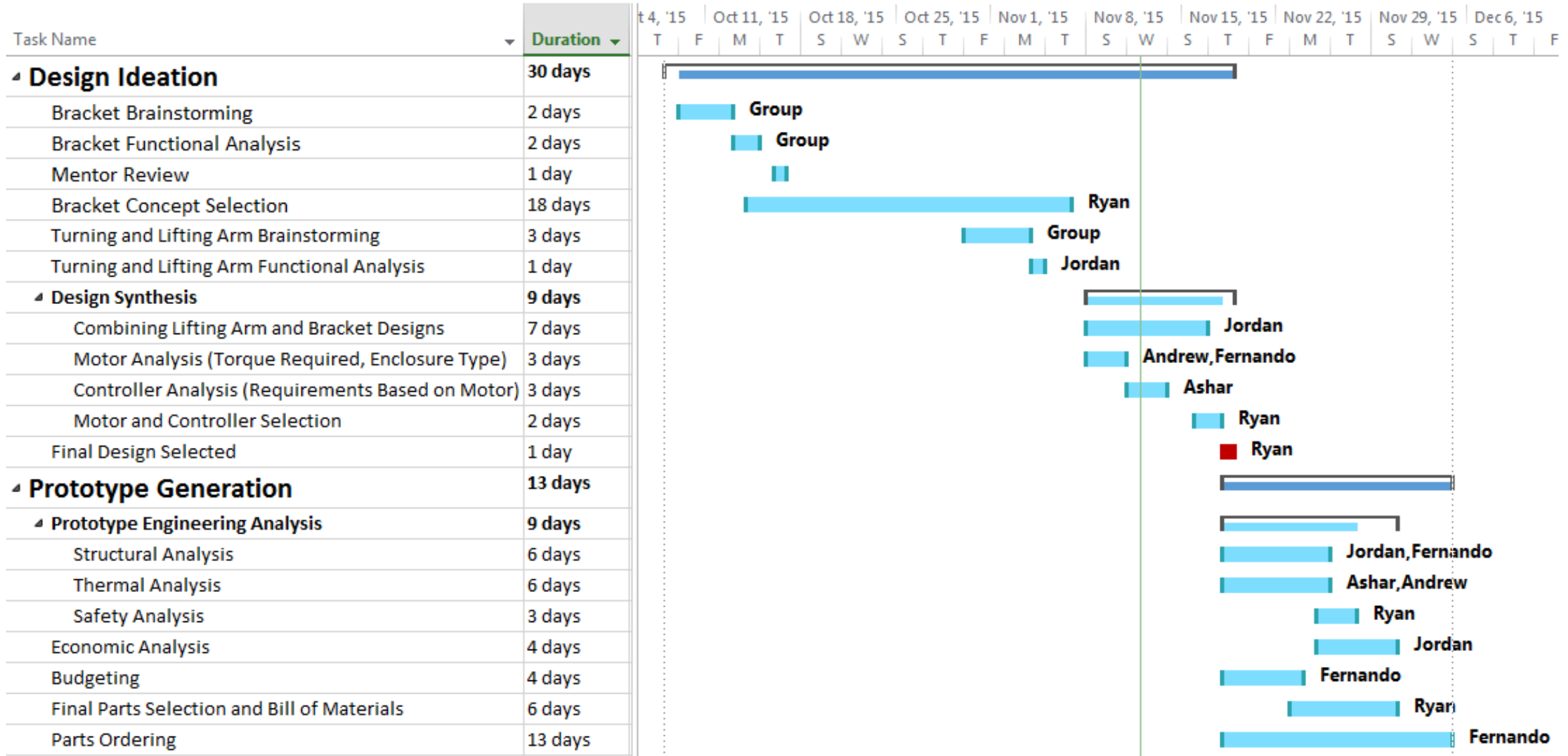
- Bracket needs to be able to turn **180** degrees in **1** second
- Required Operating Speed is **40** RPM
- To Find Required Torque from Motor
 - Assumed a very bulky bracket
 - The biggest target is attached
 - Frictionless
- Required Motor Torque: **620** ozf*in @ **40** RPM
 - Safety Factor: 1.5



Bracket: 180 Degree Positioning



Gantt Chart





Future Challenges

- Mating of the Bracket and the Arm assemblies
- Developing a suitable enclosure for the motor and control board
- Synthesis of all design components
- Engineering analysis of all design components



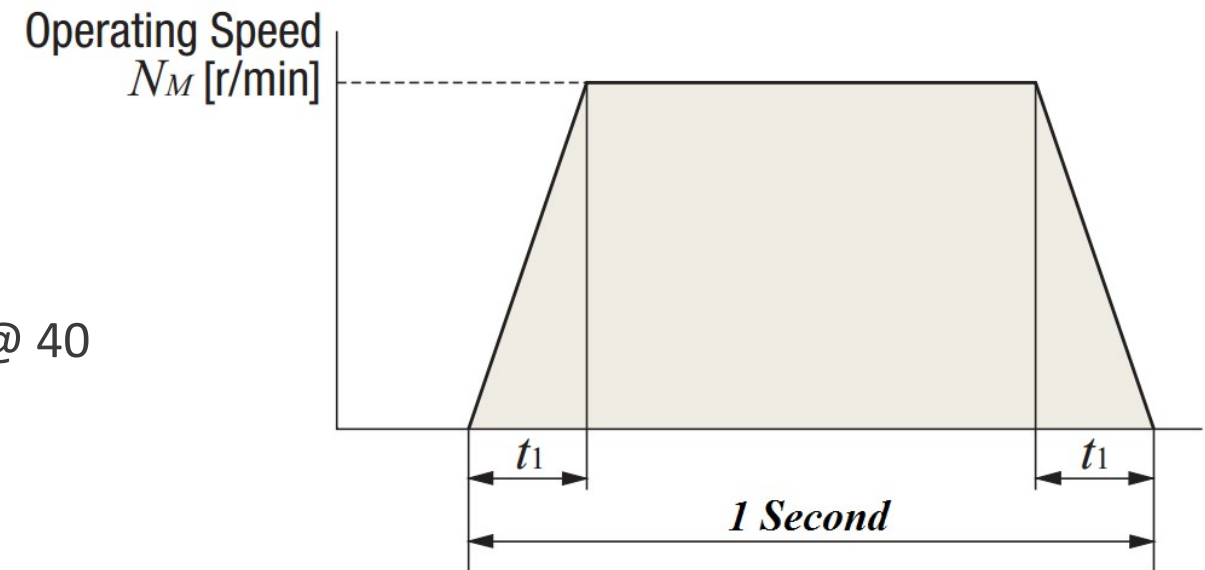
References

1. Infantry Squad Battle Course, Army Engineers
2. MS Instruments Stationary Infantry Target Specifications
3. Theissen GSA Federal Supply Schedule Price List
4. Future Army System of Integrated Targets: Presentation Devices Interface Control Doc. 2.0
5. http://www.orientalmotor.com/products/pdfs/2015/2016/H/Technical_Reference_Overview.pdf
6. McMaster Carr

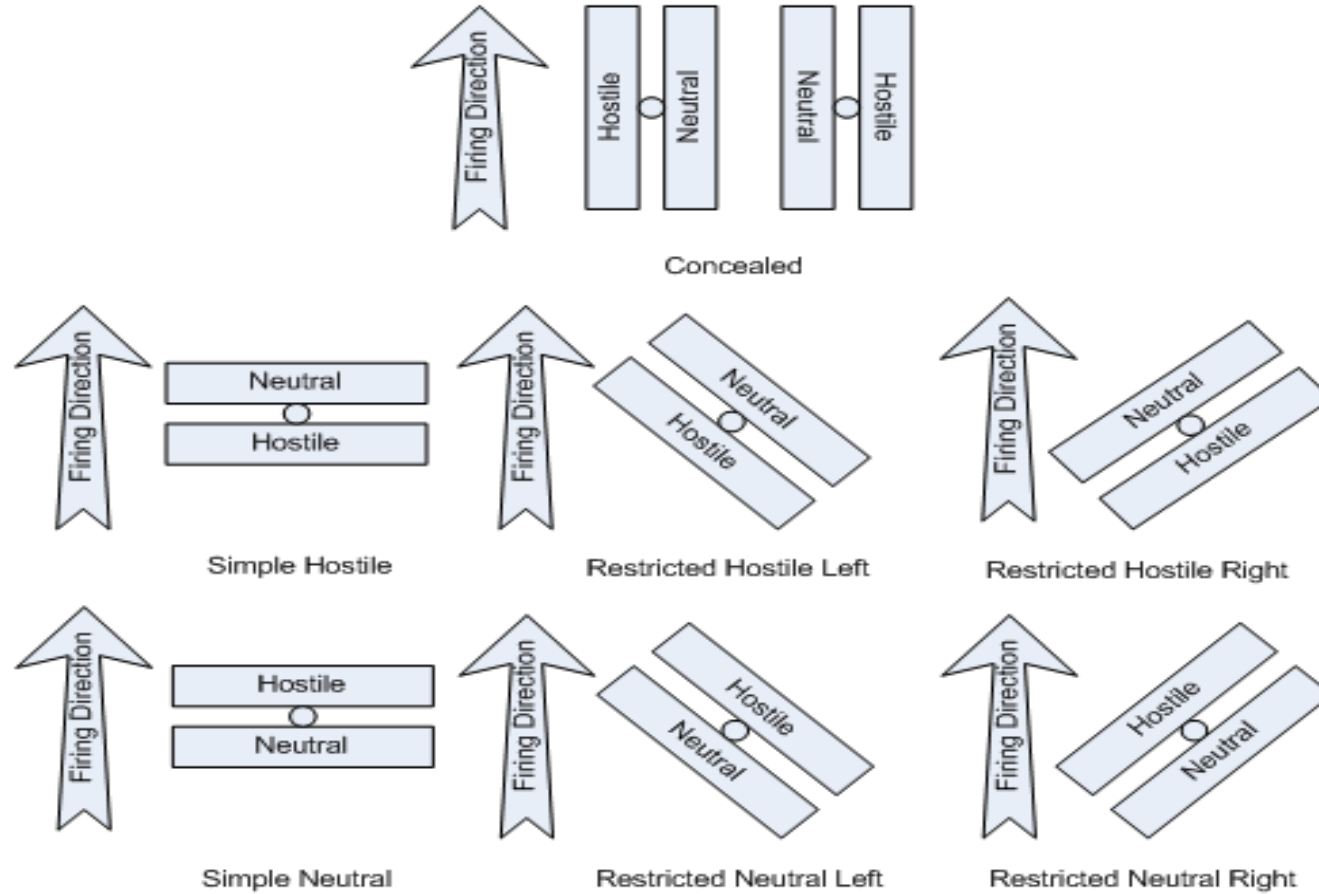
References

- Bracket needs to be able to turn **180** degrees in **1** second
- Acceleration/Deceleration time t_1 is **0.125** seconds
- To Find Required Torque from Motor
 - Assumed a very bulky bracket
 - The biggest target is attached
 - Frictionless
- Required Motor Torque: 620 ozf*in (32 lbf*in) @ 40 RPM
 - Safety Factor: 1.5

Motor Speed vs Time



References





References

FASIT 2.0 PD IDC Command	Target Action
0	Concealed
1	Simple Hostile
2	Restricted Hostile Left
3	Restricted Hostile Right
4	Simple Neutral
5	Restricted Neutral Left
6	Restricted Neutral Right

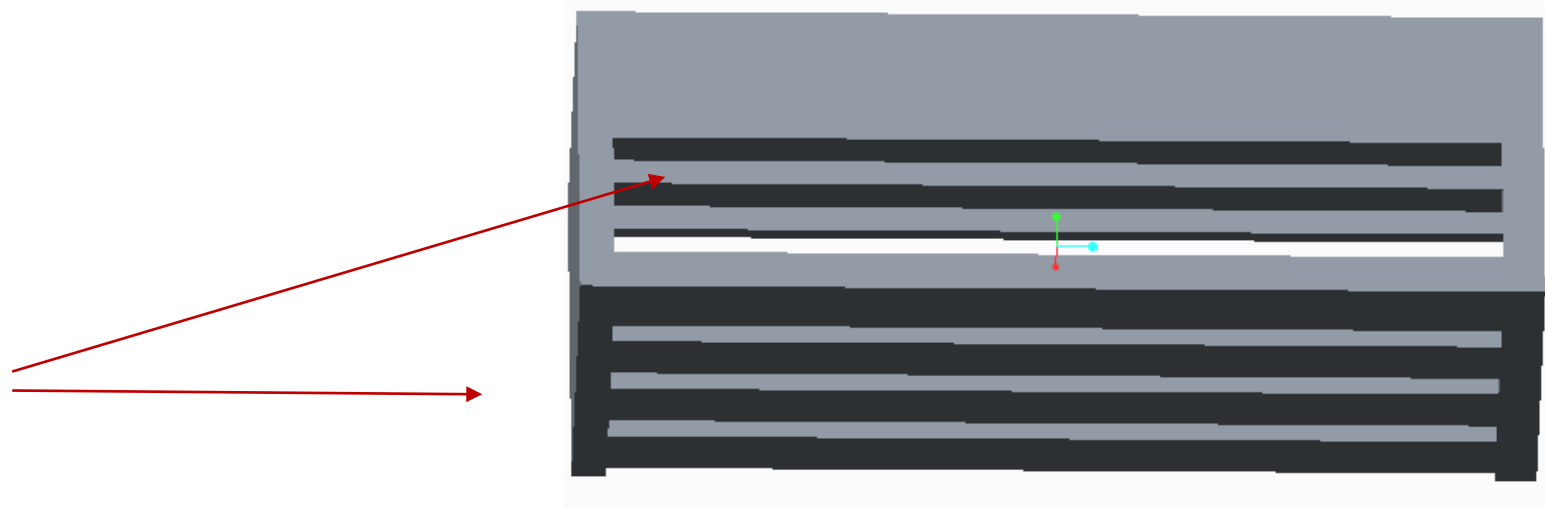
References



References

Arm Design 3:

Ventilation of
Components
Enclosure



Forces generated with tailwind

DRAG COEFF SHOULD BE 1.5

Drag Force:

$$\rho := 1.225 \frac{\text{kg}}{\text{m}^3}$$

$$v := 35 \text{mph}$$

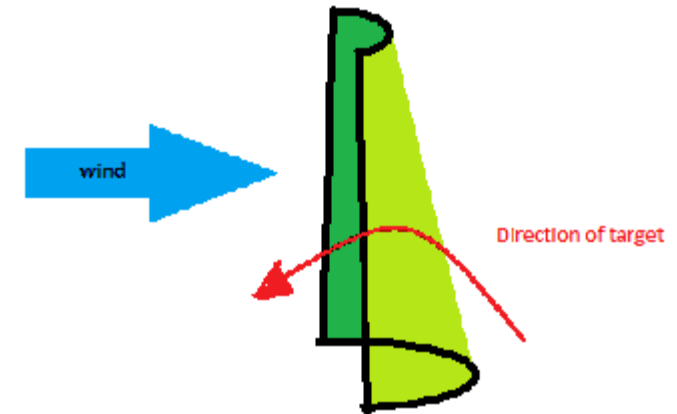
$$A := \pi \cdot 6 \text{in} \cdot 3 \text{ft} = 0.438 \text{m}^2$$

$$C_d := 2 \quad \text{this is the drag coefficient for a half sphere}$$

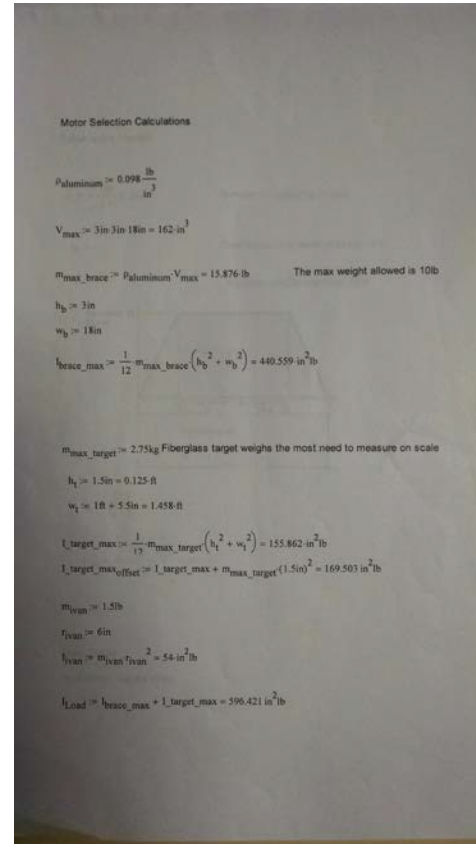
$$F_d := 0.5 \cdot \rho \cdot v^2 \cdot C_d \cdot A = 131.291 \text{N}$$

$$131 \text{N} = 29.45 \text{ lbf}$$

Note this is the force required to lower the target when a 30 mph tailwind is blowing on the back hollowed out portion.



References



References

1.8 step angle chosen

$O.P := \frac{180}{1.8} = 100$ Number of Operating Pulses

$t_0 := 1s$ Time required to perform positioning

$t_1 := .25s$ Acceleration/Deceleration Time

Operating Speed

Positioning angle $\theta = \text{[]}^\circ$

Acceleration time t_1 Deceleration time t_1

Positioning time $t_0 = \text{[]} s$

$f_2 := \frac{O.P}{t_0 - t_1} = 133.333 \frac{1}{s}$

$N_M := \frac{1.8 \cdot f_2 \cdot 60 \frac{s}{min}}{360} = 40 \frac{1}{min}$

Load Torque

No Friction, Maybe Wind

$T_L := 0$

References

Acceleration Torque

$$I_0 := 0$$

I_0 is motor inertia

$$i := 1$$

i is gear ratio

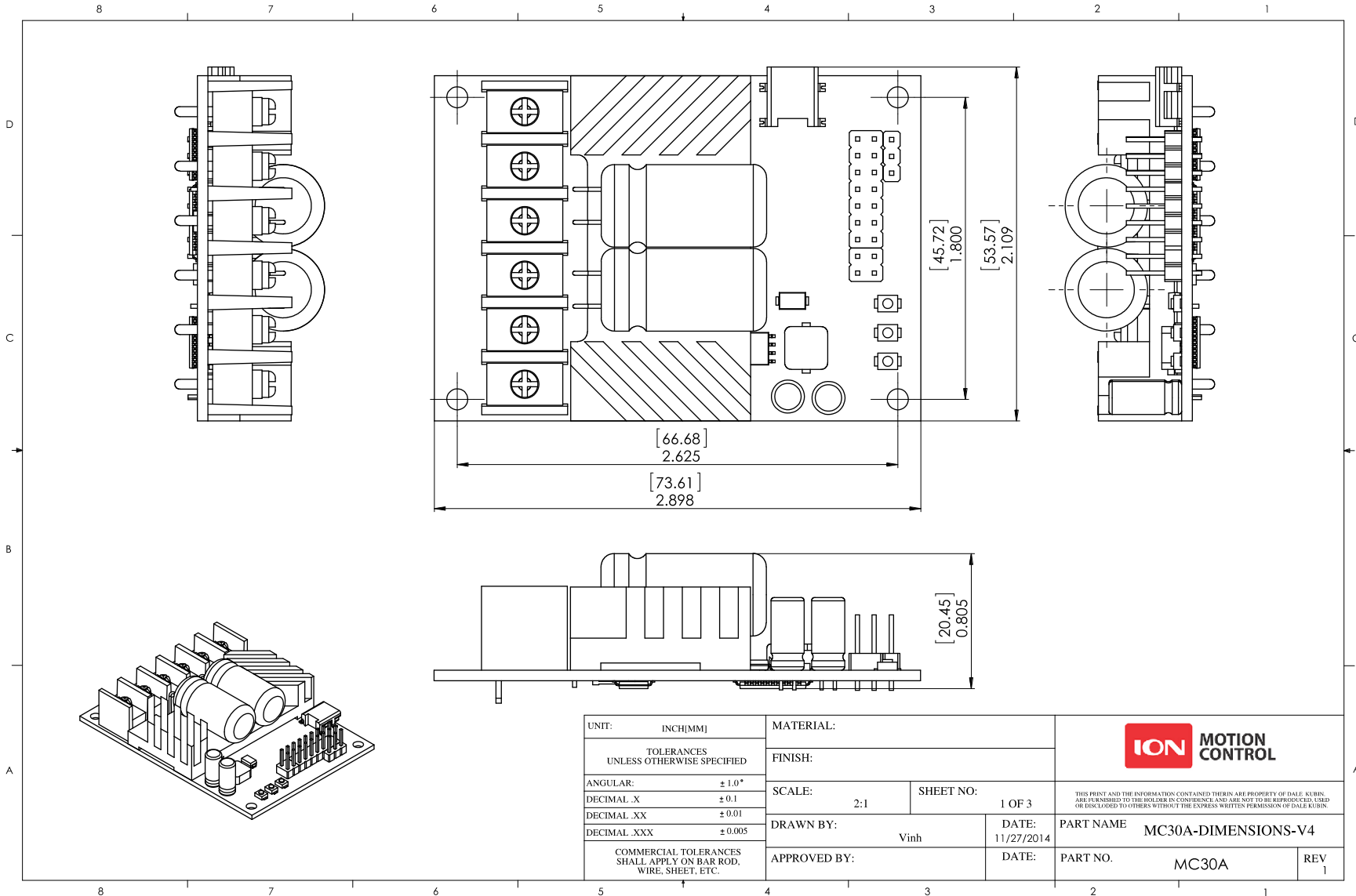
$$T_a := \frac{(I_0 \cdot i^2 + I_{\text{Load}}) \cdot (N_M \cdot 60)}{9.55 \cdot t_1} = 414.098 \text{ ozf} \cdot \text{in}$$

Required Torque

$$S_f := 1.5$$

Safety Factor

$$T_R := (T_L + T_a) \cdot S_f = 621.146 \text{ ozf} \cdot \text{in}$$



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DECIMAL .XXX	± 0.005	APPROVED BY:		DATE:	
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				REV	1